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Structural Design Details

Of

The Proposed Construction of Commercial Building
Project - MORAIS CITY MIB E BLOCK
(Business Office Building) in SF.No: 201/1E1B, 204/2B,
205/1A2 Plot No: C-6 , (L.P(R)/NTDA NO: 1/2020),
Morais City Extension -I, Keelakurichi Village &
Panchayat, Tiruverumbur Panchayats Union & Taluk,
Trichy District.

Structural Details Design by

**TRICHY RG ENGINEERING EXCELLENCE
PRIVATE LIMITED**

No. 64, Nandavanam Street,
LIC Colony
Trichy – 620021
Phone – 0431-4024691

STRUCTURAL DESIGN STABILITY CERTIFICATE.

I hereby certify that the Proposed Construction of Commercial Building Project – Morais City MIB E Block (Business Office Building) in SF.No: 201/1E1B, 204/2B, 205/1A2, Plot No: C6 ., (L.P(R)/NTDA NO: 1/2020), Morais City Extension -I, Keelakurichi Village & Panchayat, Thiruverumbur Panchayat Union & Taluk, Trichy District. The building will withstand against the Earthquake,(Seismic Zone II as per IS 1893 (Part I) 2002) loading stress parameters are within limits of National Building Code and Bureau of Indian standards code of practice for concrete and loading. The building consists of Double Basement + stilt + four floors. For external and internal partition walls 200/100 thick A. A. C block work walls are used.

The R.C.C building frame of the structure is designed as per the Indian Standard code of practice for concrete and loading as follows:

1. IS: 456-2000 Code of Practice for Plain and Reinforced concrete
2. IS: 875-1987 Code of Practice for Design loads for Buildings and structures
3. IS: 1893-2002 Criteria for Earthquakes resistant design of structures Part-1 General Provisions and Buildings
4. IS: 4326-1993 Code of Practice for Earthquakes resistant design & Construction of Buildings.
5. IS:13920-1993 Code of Practice for Ductile detailing of concrete structures subjected to seismic forces and
6. National Building code of India-2005.

It is further certified that the above structure will be constructed from foundation to roof, as per structural designs and detailing of reinforcements furnished in our drawings. The building will be **safe and Sound** as per the design.


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LPA REG NO: SE/Gr/TLPA/MAY2019/029

DESIGN BASIS REPORT

For

The Proposed Construction of Commercial Building Project – Morais City MIB E Block (Business Office Building) in SF.No: 201/1E1B, 204/2B, 205/1A2, Plot No: C6 ., (L.P(R)/NTDA NO: 1/2020), Morais City Extension -I, Keelakurichi Village & Panchayat, Thiruverumbur Panchayat Union & Taluk, Trichy District.

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1.0 OBJECTIVE

The Proposed Construction of Commercial Building Project – Morais City MIB E Block (Business Office Building) in SF.No: 201/1E1B, 204/2B, 205/1A2, Plot No: C6 ., (L.P(R)/NTDA NO: 1/2020), Morais City Extension -I, Keelakurichi Village & Panchayat, Thiruverumbur Panchayat Union & Taluk, Trichy District.

The Building is designed for Double Basement + Stilt + Four floors. The structure is supported on column in turn resting on column footing Foundation. The Structural System comprises columns, beams, slabs and wall structure.

3-D Analysis of all the building structures will be carried out using STAAD PRO Software package and analysis results shall be used for designing the various elements.

2.0 DESIGN LOADS

2.1 Dead Loads

The Deadloads that are envisaged to act permanently are considered as per **IS:875 (Part 1) – 1987 – Dead loads. Indian standard “Code of Practice for Design Loads (other than earthquakes) for Buildings and Structures”**.

1. Slab is assumed to be 125mm thick – 3.125 KN/m^2
2. Floor finish – 1.5 KN/m^2
3. AAC Block masonry walls 200mm & 100mm thick are proposed to be used (location of walls per Architectural drawings) Unit weight is taken as 8 KN/m^3
4. Weathering course in Terrace finish – 2 KN/m^2

2.2 Imposed Loads

The imposed loads that are envisaged to get permanently are considered as per **IS : 875 (part – 2) – 1987. Indian standard “Code of Practice for Design loads (other than earthquake) for Buildings and structures”**.

- | | |
|-------------------|------------------------|
| 1. Living | = 4 KN/m^2 |
| 2. Staircase | = 4 KN/m^2 |
| 3. Toilets | = 2 KN/m^2 |
| 4. Terrace floors | = 1.5 KN/m^2 |

2.3 Earthquake Load

The loading due to earthquake is assessed based on the provisions of **IS :1893-2016**. Structures with ductile detailing is considered as per **IS: 13920-2016**.

Madurai falls under Seismic Zone II

Zone factor = 0.10

Response reduction factor = 3

Importance factor = 1.0

Structure with ductile detailing is considered as per IS: 13920-2016

2.3 Load combinations

The various loads shall be combined in accordance with the stipulations in IS:875 (Part 5) – 1987. Whichever combinations produced the most unfavorable effect in the building, foundation or structural member concerned shall be adopted. The various load combinations considered in the analysis are as follows:

1. $1(DL + LL)$
2. $1(DL + 0.8LL + 0.8 SQX + 1)$
3. $1(DL + 0.8LL + 0.8 SQX - 1)$
4. $1(DL + 0.8LL + 0.8 SQZ + 1)$
5. $1(DL + 0.8LL + 0.8 SQZ - 1)$
6. $1.0(DL + SQX + 1)$
7. $1.0(DL + SQX - 1)$
8. $1.0(DL + SQZ + 1)$
9. $1.0(DL + SQZ - 1)$
10. $1.5(DL + LL)$
11. $1.5(DL + SQX + 1)$
12. $1.5(DL + SQX - 1)$
13. $1.5(DL + SQZ + 1)$
14. $1.5(DL + SQZ - 1)$
15. $1.2(DL + LL + SQX + 1)$

16. $1.2(DL + LL + SQX - 1)$
17. $1.2(DL + LL + SQZ + 1)$
18. $1.2(DL + LL + SQZ - 1)$
19. $0.9DL + 1.5SQX + 1$
20. $0.9DL + 1.5SQX - 1$
21. $0.9DL + 1.5SQZ + 1$
22. $0.9DL + 1.5SQZ - 1$

The above load combination will be considered and effect of worst combinations will be taken for design of various building elements.

3.0 ANALYSIS METHODS

The analysis of the structures is carried out using the STAAD PRO. The entire super structure is modeled using frame elements as appropriate. Beams and columns are modeled as frame elements. Appropriate loads and its combinations as per relevant IS code clauses, for most unfavorable effects are chosen for design. Various load cases considered in the analysis are briefed above.

4.0 DESIGN ASSUMPTION

- 4.1.1 The Base of the Foundation is assumed to be FIXED& PINNED.
- 4.1.2 All concrete elements shall be designed in accordance with IS 456:2000 Limit state design.
- 4.1.3 Appropriate loads and its combination as per relevant clauses, for the most unfavorable effects are chosen for design. (Refer Load Combination below).

5.0 FOUNDATION DESIGN

Type of foundation : Raft foundation
Depth of foundation : 7.5 m below natural ground level

6.0 MATERIALS

The self-weight of the various elements are computed based on the unit weight of materials as given below:

S. no	Materials	Unit weight KN / m ³
1	Reinforced Cement Concrete	25
2	AAC Block / Brick WORK(for lift well& parapet)	8/20
3	Steel	78.50

Structural concrete shall be of grade M25 for all R.c.c work.

Steel reinforcement shall be of grade Fe 500 confirming to IS : 1786-2008.

7.0 NOMINAL COVER TO REINFORCEMENT

From Durability requirement, exposure condition is assumed as mild for structural elements above ground level and moderate for structural elements below ground level.

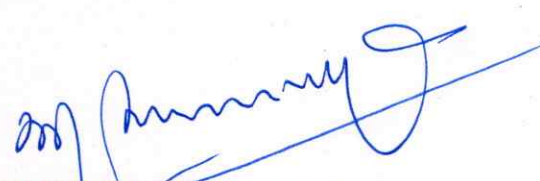
The clear cover to reinforcement to meet durability requirement shall be as follows:

Footing - 50mm

Column - 40mm

Beam- 32mm

Slab - 20mm



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Design of Isolated Footing with Moment

The values are Displayed in Blue color are the Input values

Support No = COLUMN NO C15

1 Design Forces From STAAD

Load Case = 5

- | | | |
|------------------------------------|---|---------|
| 1. Axial Load on column | = | 3800 KN |
| 2. Bending moment along x-x, M_x | = | 0 KN.m |
| 3. Bending moment along y-y, M_y | = | 0 KN.m |

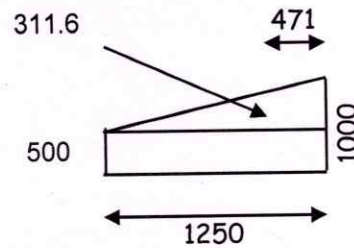
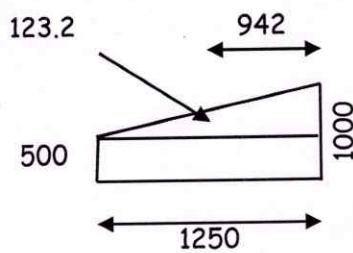
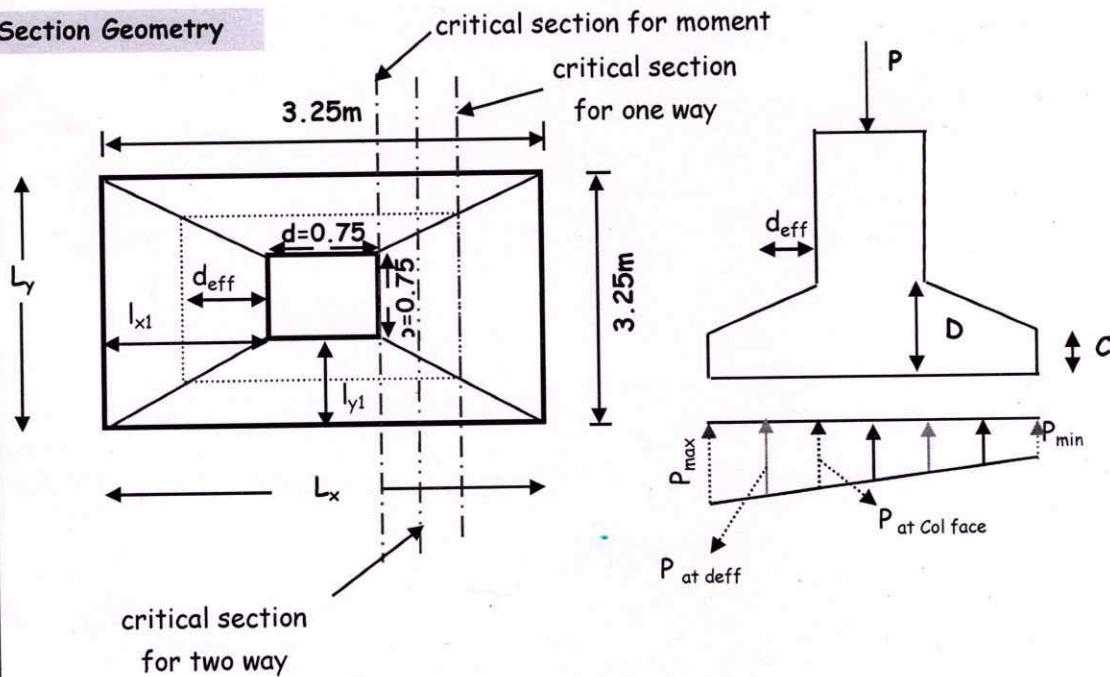
2 Design Datas

- | | | |
|---|---|-----------------------|
| 3. Compressive strength of Concrete, F_{ck} | = | 25 N/mm ² |
| 4. Yield Strength of steel, F_y | = | 500 N/mm ² |
| 5. Diameter of Reinforcement, (x-direction) | = | 16 mm |
| 6. Diameter of Reinforcement, (y-direction) | = | 16 mm |
| 7. Clear cover to the reinforcement, C | = | 50 mm |
| 8. Safe bearing capacity of soil, SBC | = | 400 KN/m ² |
| 7 Type of Footing | = | Rectangular |
| 8 Size of pedestal/Column | = | b x d |
| | = | 0.75 x 0.75 m |

2 Assume trial size of footing

- | | | |
|-----------------------------|-----|-----------------------|
| Area of footing | = | Total Load/SBC |
| Self Wt. of footing | | |
| (Assume 10% of column load) | = | 380 KN |
| Soil weight | = | 0 KN |
| Total Load | = | 4180 KN |
| Area of footing required | = | 4180 / 400 |
| | = | 10.45 m ² |
| Size Required | B = | 3.2 m |
| | L = | 3.2 m |
| Size Provided | B = | 3.25 m |
| | L = | 3.25 m |
| Area of Footing Provided | = | 10.563 m ² |
| | | 10.5625 > 10.45 |
| | | O.K |

3 Section Geometry



$$\begin{aligned}
 l_{x1} &= (L_x - d)/2 \\
 &= (3.25 - 0.75)/2 \\
 &= 1.25 \text{ m} \\
 l_{y1} &= (L_y - d)/2 \\
 &= (3.25 - 0.75)/2 \\
 &= 1.25 \text{ m}
 \end{aligned}$$

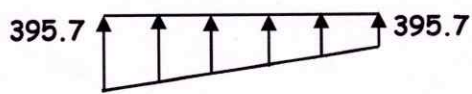
Assume Overall depth of footing, D
 Depth at free end, C
 d_{eff} at critical moment section
 d_{eff} at critical one way shear section
 d_{eff} at critical two way shear section

$$\begin{aligned}
 &= 1000 \text{ mm} \\
 &= 500 \text{ mm} \\
 &= 942 \text{ mm} \\
 &= 565.2 \text{ mm} \\
 &= 753.6 \text{ mm}
 \end{aligned}$$

4 Check for Soil Pressure

A) Along X direction

Eccentricity, e_{xx}



$$\begin{aligned} &= (M_{xx}/P) \\ &= 0 / 4180 \\ &= 0 \text{ m} \\ L_x/6 &= 0.542 \text{ m} \\ 0.542 > 0 \\ &\mathbf{e_{xx} < L_x/6} \end{aligned}$$

Maximum Pressure, P_{max}

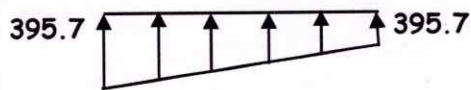
$$\begin{aligned} &= P/A(1+6e/B) \\ &= 4180/10.5625(1 + 6 \times (0+0)/3.25) \\ &= \mathbf{395.7 \text{ KN/m}^2} \\ 395.7 < 400 \\ &\mathbf{Safe} \end{aligned}$$

Minimum Pressure, P_{min}

$$\begin{aligned} &= P/A(1-6e/B) \\ &= 4180/10.5625(1 - 6 \times (0+0)/3.25) \\ &= \mathbf{395.7 \text{ KN/m}^2} \\ 395.7 < 400 \\ &\mathbf{Safe} \end{aligned}$$

B) Along Y direction

Eccentricity, e_{yy}



$$\begin{aligned} &= (M_{yy}/P) \\ &= 0 / 4180 \\ &= 0 \text{ m} \\ L_y/6 &= 0.542 \text{ m} \\ 0.542 > 0 \\ &\mathbf{e_{yy} < L_y/6} \end{aligned}$$

Maximum Pressure, P_{max}

$$\begin{aligned} &= (P/A(1+6e/B)) \\ &= 4180/10.5625(1 + 6 \times (0+0)/3.25) \\ &= \mathbf{395.7 \text{ KN/m}^2} \\ 395.7 < 400 \\ &\mathbf{Safe} \end{aligned}$$

Minimum Pressure, P_{min}

$$\begin{aligned} &= P/A(1-6e/B) \\ &= 4180/10.5625(1 - 6 \times (0+0)/3.25) \\ &= \mathbf{395.7 \text{ KN/m}^2} \\ 395.7 < 400 \\ &\mathbf{Safe} \end{aligned}$$

5 Bending moment calculations

S.No	Direction	Pmax(net)	Pmin(net)	P at face of the column	Moment, KN/m
1	x	359.72	359.72	359.72	421.545
2	y	359.72	359.72	359.72	421.545

6 Check for depth (Moment consideration)

$$\begin{aligned} \mu_{u,lim} &= (0.36 \times F_{ck} \times (x_{u,max}/d) \times (1 - 0.42(x_{u,max}/d)) \times b d^2 \\ x_{u,max}/d &= 0.46 \\ \mu_{u,lim} &= 3.34 b d^2 \\ d_{reqd} &= (\mu_{u,lim}/Q_b)^{1/2} \\ &= (421545000/(3.34 \times 1000))^{1/2} \\ &= 355.26 \text{ mm} \\ 355.26 &< 942 \\ &\text{O.K} \end{aligned}$$

7 Calculation of Reinforcement

S. N	Direction	μ_u/bd^2	pt from SP16	pt, min	pt, provided	Ast, mm ²
1	x	0.48	0.113	0.12	0.120	1130.4
2	y	0.48	0.113	0.12	0.120	1130.4

$$\begin{aligned} pt &= 100A_{st}/bd \\ A_{st} &= (pt/100) \times bd \end{aligned}$$

8 Spacing of reinforcement

Spacing, mm		Spacing provided, mm	Ast provided, mm ²
Reqd	Minimum		
177	300	125	1607.68
177	300	125	1607.68

$$\text{Spacing} = (ast \times 1000)/A_{st}$$

where,
ast = C/s area of bar
Ast = Area of reinforcement provided

$$pt_{max, Provided} = 0.1707 \%$$

9 Check for one way shear

S.No	Direction	Pmax(net)	Pmin(net)	P at critical 1way shear Xn	Shear, KN
1	x	359.72	359.72	359.72	166.185
2	y	359.72	359.72	359.72	166.185

$$\text{Nominal Shear stress, } \tau_v = V_u/bd$$

$$\begin{aligned}
 &= 166185/1000 \times 565.2 \\
 &= 0.29 \text{ N/mm}^2 \\
 \text{pt.max, Provided} &= 0.1707 \% \\
 \text{Allowable shear stress, } t_c \text{ (for pt,max)} &= 0.3082 \text{ N/mm}^2 \\
 &t_v < t_c \\
 &\text{O.K}
 \end{aligned}$$

10 Check for two way Shear

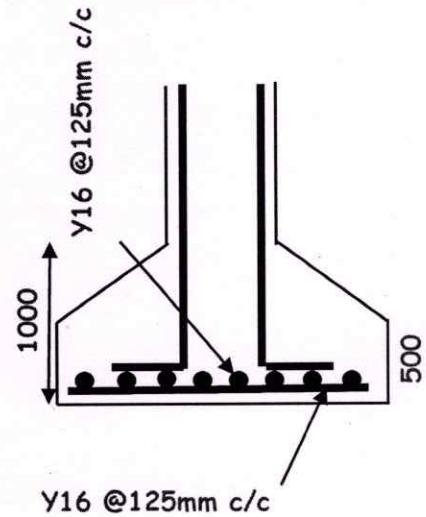
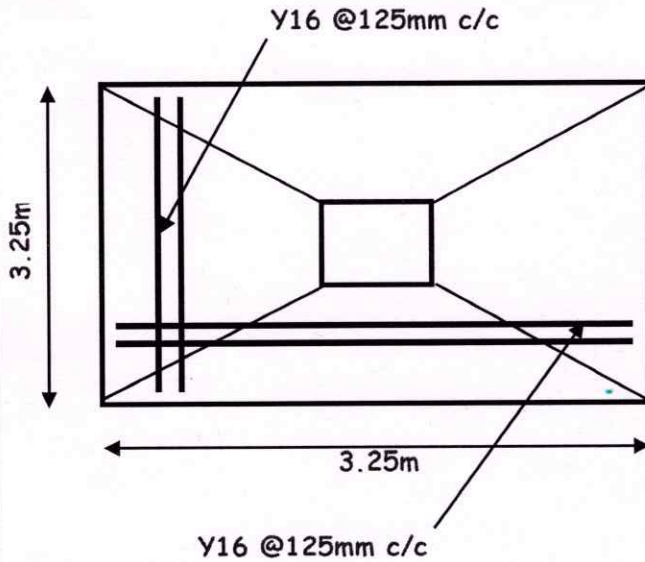
$$\begin{aligned}
 \text{Punching Shear, } V_u &= \text{Net upward pressure} \times (A_F - A_c) \\
 &= 5396.445 \text{ KN} \\
 \text{Punching Shear stress,} &= V_u / \text{perimeter at critical section} \times d_{\text{eff}} \\
 &= 1.0581 \text{ N/mm}^2 \\
 \text{Allowable Stress} &= 0.25(f_{ck})^{1/2} \\
 &= 1.25 \text{ N/mm}^2 \\
 &\text{O.K}
 \end{aligned}$$

11 Check for bearing stress

$$\begin{aligned}
 \text{Actual bearing stress,} &= 5700 \text{ KN} \\
 \text{Limiting bearing stress @ Column - footing} \\
 \text{interface, } f_{br,\text{max}} &= 0.45 f_{ck} (A_1/A_2)^{1/2} \\
 A_1 &= 902500 \text{ mm}^2 \\
 (A_1/A_2)^{1/2} &= 1 \\
 f_{br,\text{max}} &= 11.25 \text{ N/mm}^2 \\
 \text{Limiting bearing stress @ Column - footing} \\
 \text{interface, } f_{br,\text{max}} &= 0.45 f_{ck} (A_1/A_2)^{1/2} \\
 A_1 &= 10562500 \text{ mm}^2 \\
 A_2 &= 902500 \text{ mm}^2 \\
 (A_1/A_2)^{1/2} &= 2 \\
 f_{br,\text{max}} &= 22.5 \text{ N/mm}^2 \\
 \text{Limiting Bearing resistance, } F_{br} &= 10153 \text{ KN} \\
 &= 10153.125 > 5700 \\
 &\text{O.K} \\
 0 &= 0 \\
 0 &= 0 \\
 0 &= 0 \emptyset
 \end{aligned}$$

11 Reinforcement Details

Direction	Reinforcement
X	Y16 @125mm c/c
Y	Y16 @125mm c/c



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Design of column with Biaxial Moment

Column No = C15 (up to stilt roof)

1 Design Forces From STAAD

Load Case = C10

- | | | |
|---------------------------------------|---|----------|
| 1. Axial Load on column | = | 4390 KN |
| 2. Bending moment along x-x, M_{ux} | = | 138 KN.m |
| 3. Bending moment along y-y, M_{uy} | = | 58 KN.m |

2 Design Datas

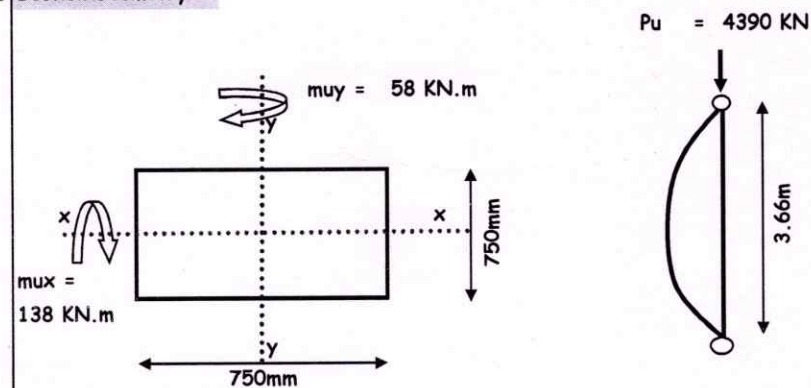
- | | | |
|--|---|-----------------------|
| 1. Compressive strength of Concrete, F_{ck} | = | 25 N/mm ² |
| 2. Yield Strength of steel, F_y | = | 500 N/mm ² |
| 3. Diameter of Longitudinal Reinforcement, | = | 32 mm |
| 4. Diameter of lateral Reinforcement, | = | 10 mm |
| 5. Clear cover to the reinforcement, C | = | 32 mm |
| 6. Type of column | = | Rectangular |
| 7. Size of Column | = | $b \times d$ |
| | = | 750 x 750 mm |
| 8. Unsupported Length of Column along x-x, L_x | = | 3.66 m |
| 9. Unsupported Length of Column along y-y, L_y | = | 3.66 m |
| 10. Effective length factor, | = | 1 |
| 11. Effective Length of Column, along x-x, L_x | = | 3.66 m |
| 12. Effective Length of Column, along y-y, L_y | = | 3.66 m |

2 Check for l_{eff}/D

- | | | |
|--|---|--------------|
| Effective length, l_{ex} /Lateral dimensions | = | L_{ex} / D |
| | = | 4.88 |
| | = | $4.88 < 12$ |
| | = | Short Column |

- | | | |
|--|---|--------------|
| Effective length, l_{ey} /Lateral dimensions | = | L_{ey} / b |
| | = | 4.88 |
| | = | $4.88 < 12$ |
| | = | Short Column |

3 Section Geometry



4 Check for Minimum Eccentricity

Applied eccentricities

- | | | |
|-------|---|----------------|
| e_x | = | M_{ux} / P_u |
| | = | $138 / 4390$ |
| | = | 31.435 mm |
| e_y | = | M_{uy} / P_u |
| | = | $58 / 4390$ |
| | = | 13.212 mm |

As per clause
25.1.2.2,
IS:456:2000

As per Clause 25.4,
IS:456:2000

Minimum eccentricity

$$\begin{aligned}e_{xx} &= (l_{ex}/500) + (D/30) \\&= (3660/500) + (750/30) \\&= 32.32 \text{ mm or } 20 \text{ mm} \\&= 32.32 \text{ mm} \\e_{yy} &= (l_{ey}/500) + (D/30) \\&= (3660/500) + (750/30) \\&= 32.32 \text{ mm or } 20 \text{ mm} \\&= 32.32 \text{ mm}\end{aligned}$$

5 Moment due to Eccentricity

$$\begin{aligned}m_{uex} &= P_u \times e_{xx} \\&= (4390 \times 32.32)/1000 \\&= 141.88 \text{ KN.m}\end{aligned}$$

$$\begin{aligned}m_{uey} &= P_u \times e_{yy} \\&= (4390 \times 32.32)/1000 \\&= 141.88 \text{ KN.m}\end{aligned}$$

6 Design Moment

$$\begin{aligned}m_{ux} &= M_{ux} \text{ or } m_{uex} \\&= 141.88 \text{ KN.m}\end{aligned}$$

$$\begin{aligned}m_{uy} &= M_{uy} \text{ or } m_{uey} \\&= 141.88 \text{ KN.m}\end{aligned}$$

7 Calculation of Longitudinal reinforcement

$$\begin{aligned}\text{Assume percentage of reinforcement} &= 2.2 \% \\A_{sc, \text{ required}} &= 2.2/100 \times 750 \times 750 \\&= 12375 \text{ mm}^2 \\ \text{No of bars} &= 16 \text{ Nos} \\A_{sc, \text{ Provided}} &= 12861 \text{ mm}^2 \\p_t, \text{ provided} &= 2.286 \%\end{aligned}$$

Moment Capacity Along x Direction

$$\begin{aligned}(P_u/f_{ck} b D) &= (4390000/25 \times 750 \times 750) \\&= 0.31 \\p/f_{ck} &= 2.286/25 \\&= 0.09\end{aligned}$$

$$\begin{aligned}d'/D &= 32/750 \\&= 0.04\end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{ux1}/f_{ck} b D^2 &= 0.16 \\ M_{ux1} &= 0.16 \times 750 \times 750 \times 750 \times 25 \\ &= 1687.5 \text{ KN.m} \end{aligned}$$

Moment Capacity Along y Direction

$$\begin{aligned} (P_u/f_{ck} b D) &= (4390000/25 \times 750 \times 750) \\ &= 0.31 \end{aligned}$$

$$\begin{aligned} p/f_{ck} &= 2.286/25 \\ &= 0.0914 \\ b'/D &= 32/750 \\ &= 0.04 \end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{uy1}/f_{ck} b D^2 &= 0.16 \\ M_{uy1} &= 0.16 \times 750 \times 750 \times 750 \times 25 \\ &= 1687.5 \text{ KN.m} \end{aligned}$$

8 Check for Moment Capacity

$$(M_{ux}/M_{ux1})^{\alpha_n} + (M_{uy}/M_{uy1})^{\alpha_n} < 1$$

$$\begin{aligned} P_{uz} &= (0.45 f_{ck} A_c) + (0.75 f_y - 0.45 f_{ck}) A_{sc} \\ A_c &= 562500 \text{ mm}^2 \\ P_{uz} &= 11006.314 \text{ KN} \\ P_u/P_{uz} &= 0.399 \\ \alpha_n &= 1.3317 \end{aligned}$$

For $P_u/P_{uz} = 0.2$ to 0.8
 α_n varies from 1.0 to 2.0

$$\begin{aligned} (M_{ux}/M_{ux1})^{\alpha_n} + (M_{uy}/M_{uy1})^{\alpha_n} &= 0.074 \\ 0.074 &< 1 \end{aligned}$$

O.K

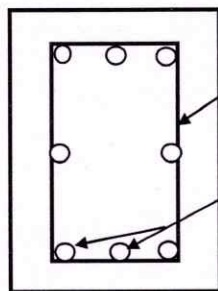
9 Calculation of Lateral Reinforcement

Spacing of ties

1. Least Lateral Dimensions of column = 750 mm
2. Sixteen times the least dia of Longi bar = 512 mm
3. 300mm = 300 mm

$$\text{Adopt Spacing} = 300 \text{ mm}$$

10 Details



Y10@300mm c/c

No of bars = 16 Nos

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LPA REG NO: SE/Gr/TLPA/MAY2019/029

Design of column with Biaxial Moment

Column No = C15 (Stilt roof to Third floor roof)

1 Design Forces From STAAD

Load Case = C5

1. Axial Load on column = 2580 KN
2. Bending moment along x-x, M_{ux} = 89 KN.m
3. Bending moment along y-y, M_{uy} = 62 KN.m

2 Design Datas

1. Compressive strength of Concrete, F_{ck} = 25 N/mm²
2. Yield Strength of steel, F_y = 500 N/mm²
3. Diameter of Longitudinal Reinforcement, = 32 mm
4. Diameter of lateral Reinforcement, = 8 mm
5. Clear cover to the reinforcement, C = 32 mm
6. Type of column = Rectangular
7. Size of Column = $b \times d$ = 750 x 750 mm
8. Unsupported Length of Column along x-x, L_x = 3.66 m
9. Unsupported Length of Column along y-y, L_y = 3.66 m
10. Effective length factor, = 1
11. Effective Length of Column, along x-x, L_{ex} = 3.66 m
12. Effective Length of Column, along y-y, L_y = 3.66 m

2 Check for l_{eff}/D

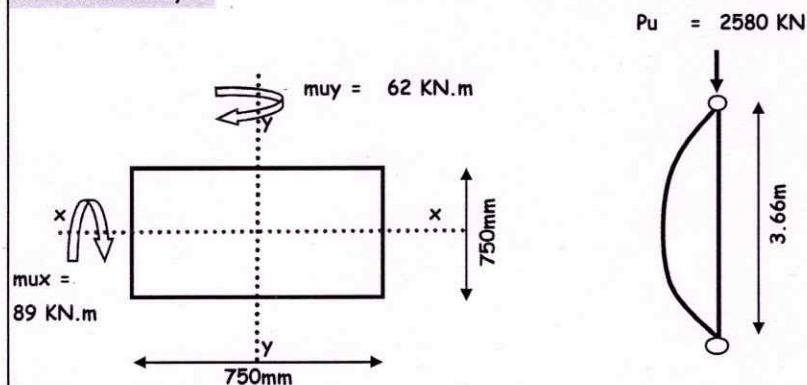
- Effective length, l_{ex} /Lateral dimensions
- = L_{ex} / D
 - = 4.88
 - = $4.88 < 12$
 - = Short Column

Effective length, l_{ey} /Lateral dimensions

- = L_{ex} / b
- = 4.88
- = $4.88 < 12$
- = Short Column

As per clause
25.1.2.2,
IS:456:2000

3 Section Geometry



4 Check for Minimum Eccentricity

Applied eccentricities

- $e_x = M_{ux} / P_u$
- = $89 / 2580$
- = 34.496 mm
- $e_y = M_{uy} / P_u$
- = $62 / 2580$
- = 24.031 mm

As per Clause 25.4,
IS:456:2000

Minimum eccentricity

$$\begin{aligned}e_{xx} &= (l_e x / 500) + (D / 30) \\&= (3660 / 500) + (750 / 30) \\&= 32.32 \text{ mm or } 20 \text{ mm} \\&= 32.32 \text{ mm} \\e_{yy} &= (l_e y / 500) + (D / 30) \\&= (3660 / 500) + (750 / 30) \\&= 32.32 \text{ mm or } 20 \text{ mm} \\&= 32.32 \text{ mm}\end{aligned}$$

5 Moment due to Eccentricity

$$\begin{aligned}m_{uex} &= P_u \times e_{xx} \\&= (2580 \times 32.32) / 1000 \\&= 83.39 \text{ KN.m}\end{aligned}$$

$$\begin{aligned}m_{uey} &= P_u \times e_{yy} \\&= (2580 \times 32.32) / 1000 \\&= 83.39 \text{ KN.m}\end{aligned}$$

6 Design Moment

$$\begin{aligned}m_{ux} &= M_{ux} \text{ or } m_{uex} \\&= 89 \text{ KN.m}\end{aligned}$$

$$\begin{aligned}m_{uy} &= M_{uy} \text{ or } m_{uey} \\&= 83.39 \text{ KN.m}\end{aligned}$$

7 Calculation of Longitudinal reinforcement

$$\begin{aligned}\text{Assume percentage of reinforcement} &= 1.6 \% \\ \text{Asc, required} &= 1.6 / 100 \times 750 \times 750 \\&= 9000 \text{ mm}^2 \\ \text{No of bars} &= 12 \text{ Nos} \\ \text{Asc, Provided} &= 9646 \text{ mm}^2 \\ \text{pt, provided} &= 1.715 \%\end{aligned}$$

Moment Capacity Along x Direction

$$\begin{aligned}(P_u / f_{ck} b D) &= (2580000 / 25 \times 750 \times 750) \\&= 0.18 \\ p / f_{ck} &= 1.715 / 25 \\&= 0.07\end{aligned}$$

$$\begin{aligned}d' / D &= 32 / 750 \\&= 0.04\end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{ux1}/f_{ck} b D^2 &= 0.16 \\ M_{ux1} &= 0.16 \times 750 \times 750 \times 750 \times 25 \\ &= 1687.5 \text{ KN.m} \end{aligned}$$

Moment Capacity Along y Direction

$$\begin{aligned} (P_u/f_{ck} b D) &= (2580000/25 \times 750 \times 750) \\ &= 0.18 \end{aligned}$$

$$\begin{aligned} p/f_{ck} &= 1.715/25 \\ &= 0.0686 \\ b'/D &= 32/750 \\ &= 0.04 \end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{uy1}/f_{ck} b D^2 &= 0.16 \\ M_{uy1} &= 0.16 \times 750 \times 750 \times 750 \times 25 \\ &= 1687.5 \text{ KN.m} \end{aligned}$$

8 Check for Moment Capacity

$$(M_{ux}/M_{ux1})^{an} + (M_{uy}/M_{uy1})^{an} < 1$$

$$\begin{aligned} P_{uz} &= (0.45 f_{ck} A_c) + (0.75 f_y - 0.45 f_{ck}) A_{sc} \\ A_c &= 562500 \text{ mm}^2 \\ P_{uz} &= 9836.8575 \text{ KN} \\ P_u/P_{uz} &= 0.262 \\ an &= 1.1033 \end{aligned}$$

For $P_u/P_{uz} = 0.2$ to 0.8
an varies from 1.0 to 2.0

$$\begin{aligned} (M_{ux}/M_{ux1})^{an} + (M_{uy}/M_{uy1})^{an} &= 0.075 \\ 0.075 &< 1 \end{aligned}$$

O.K

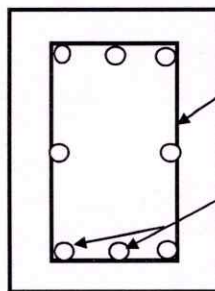
9 Calculation of Lateral Reinforcement

Spacing of ties

1. Least Lateral Dimensions of column = 750 mm
2. Sixteen times the least dia of Longi bar = 512 mm
3. 300mm = 300 mm

Adopt Spacing = 300 mm

10 Details



Y8@300mm c/c

No of bars = 16 Nos

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LPA REG NO: SE/Gr/TLPA/MAY2019/029

Design of column with Biaxial Moment

Column No = C45 (third floor roof to terrace)

Load Case = C5

1 Design Forces From STAAD

- | | | |
|---------------------------------------|---|---------|
| 1. Axial Load on column | = | 780 KN |
| 2. Bending moment along x-x, M_{ux} | = | 54 KN.m |
| 3. Bending moment along y-y, M_{uy} | = | 26 KN.m |

2 Design Datas

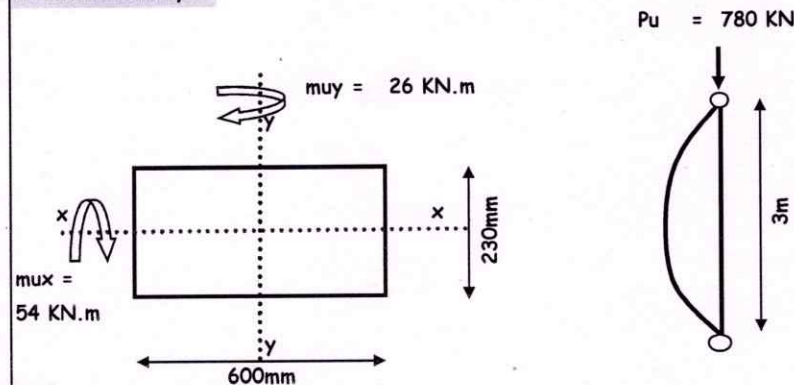
- | | | |
|---|---|-----------------------|
| 1. Compressive strength of Concrete, F_{ck} | = | 25 N/mm ² |
| 2. Yield Strength of steel, F_y | = | 500 N/mm ² |
| 3. Diameter of Longitudinal Reinforcement, | = | 16 mm |
| 4. Diameter of lateral Reinforcement, | = | 8 mm |
| 5. Clear cover to the reinforcement, C | = | 32 mm |
| 6. Type of column | = | Rectangular |
| 7. Size of Column | = | $b \times d$ |
| | = | 230 x 600 mm |
| 8. Unsupported Length of Column along x-x, L_x | = | 3 m |
| 9. Unsupported Length of Column along y-y, L_y | = | 3 m |
| 10. Effective length factor, | = | 1 |
| 11. Effective Length of Column, along x-x, L_{ex} | = | 3 m |
| 12. Effective Length of Column, along y-y, L_{ey} | = | 3 m |

2 Check for l_{eff}/D

- | | | |
|---|---|--------------|
| Effective length, l_{ex} / Lateral dimensions | = | L_{ex} / D |
| | = | 13.04 |
| | = | $13.04 > 12$ |
| | = | Long Column |

- | | | |
|---|---|--------------|
| Effective length, l_{ey} / Lateral dimensions | = | L_{ey} / b |
| | = | 5 |
| | = | $5 < 12$ |
| | = | Short Column |

3 Section Geometry



4 Check for Minimum Eccentricity

- | | |
|------------------------|------------------|
| Applied eccentricities | |
| e_x | = M_{ux} / P_u |
| | = $54 / 780$ |
| | = 69.231 mm |
| e_y | = M_{uy} / P_u |
| | = $26 / 780$ |
| | = 33.333 mm |

As per clause
25.1.2.2,
IS:456:2000

As per Clause 25.4,
IS:456:2000

Minimum eccentricity

$$\begin{aligned}e_{xx} &= (l_{ex}/500) + (D/30) \\&= (3000/500) + (600/30) \\&= 26 \text{ mm or } 20 \text{ mm} \\&= 26 \text{ mm} \\e_{yy} &= (l_{ey}/500) + (D/30) \\&= (3000/500) + (230/30) \\&= 13.667 \text{ mm or } 20 \text{ mm} \\&= 20 \text{ mm}\end{aligned}$$

5 Moment due to Eccentricity

$$\begin{aligned}m_{uex} &= P_u \times e_{xx} \\&= (780 \times 26)/1000 \\&= 20.28 \text{ KN.m} \\m_{uey} &= P_u \times e_{yy} \\&= (780 \times 13.67)/1000 \\&= 10.66 \text{ KN.m}\end{aligned}$$

6 Design Moment

$$\begin{aligned}m_{ux} &= M_{ux} \text{ or } m_{uex} \\&= 54 \text{ KN.m} \\m_{uy} &= M_{ux} \text{ or } m_{uey} \\&= 26 \text{ KN.m}\end{aligned}$$

7 Calculation of Longitudinal reinforcement

$$\begin{aligned}\text{Assume percentage of reinforcement} &= 1.2 \% \\A_{sc, \text{ required}} &= 1.2/100 \times 230 \times 600 \\&= 1656 \text{ mm}^2 \\ \text{No of bars} &= 9 \text{ Nos} \\A_{sc, \text{ Provided}} &= 1809 \text{ mm}^2 \\p_t, \text{ provided} &= 1.311 \%\end{aligned}$$

Moment Capacity Along x Direction

$$\begin{aligned}(P_u/f_{ck} b D) &= (780000/25 \times 230 \times 600) \\&= 0.23 \\p/f_{ck} &= 1.311/25 \\&= 0.05 \\d'/D &= 32/600 \\&= 0.05\end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{ux1}/f_{ck} b D^2 &= 0.11 \\ M_{ux1} &= 0.11 \times 230 \times 230 \times 600 \times 25 \\ &= 227.7 \text{ KN.m} \end{aligned}$$

Moment Capacity Along y Direction

$$\begin{aligned} (P_u/f_{ck} b D) &= (780000/25 \times 230 \times 600) \\ &= 0.23 \end{aligned}$$

$$\begin{aligned} p/f_{ck} &= 1.311/25 \\ &= 0.0524 \\ b'/D &= 32/230 \\ &= 0.14 \end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{uy1}/f_{ck} b D^2 &= 0.1 \\ M_{uy1} &= 0.1 \times 230 \times 230 \times 600 \times 25 \\ &= 207 \text{ KN.m} \end{aligned}$$

8 Check for Moment Capacity

$$(M_{ux}/M_{ux1})^{an} + (M_{uy}/M_{uy1})^{an} < 1$$

$$\begin{aligned} P_{uz} &= (0.45 f_{ck} A_c) + (0.75 f_y - 0.45 f_{ck}) A_{sc} \\ A_c &= 138000 \text{ mm}^2 \\ P_{uz} &= 2210.5238 \text{ KN} \\ P_u/P_{uz} &= 0.353 \\ an &= 1.255 \end{aligned}$$

For $P_u/P_{uz} = 0.2$ to 0.8
an varies from 1.0 to 2.0

$$\begin{aligned} (M_{ux}/M_{ux1})^{an} + (M_{uy}/M_{uy1})^{an} &= 0.238 \\ &0.238 < 1 \end{aligned}$$

O.K

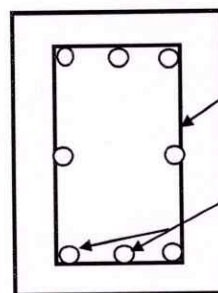
9 Calculation of Lateral Reinforcement

Spacing of ties

1. Least Lateral Dimensions of column = 230 mm
2. Sixteen times the least dia of Longi bar = 256 mm
3. 300mm = 300 mm

$$\text{Adopt Spacing} = 200 \text{ mm}$$

10 Details



Y8@200mm c/c

$$\text{No of bars} = 8 \text{ Nos}$$

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LPA REG NO: SE/Gr/TLPA/MAY2019/029

Design of Beam BB1

Size of Beam	- 340mm x 750mm
Concrete grade	- M25
Characteristic strength of reinforcement	- 500N/mm ²
Clear cover	- 32 mm,
Effective depth = $750-32-25/2 = 702$	- 702 mm
Dia of rod used	- 25 mm

From staadd out put result

Factored Shear force maximum	- 374 kN
Factored Sagging moment M_u	- 491 knm
Factored Hogging moment M_u	- 793 knm

Reinforcement is at bottom:

$$M_u/bd^2 \text{ (sagging)} = = \frac{491 \times 10^6}{340 \times (702)^2} = 2.93 \text{ N/mm}^2$$

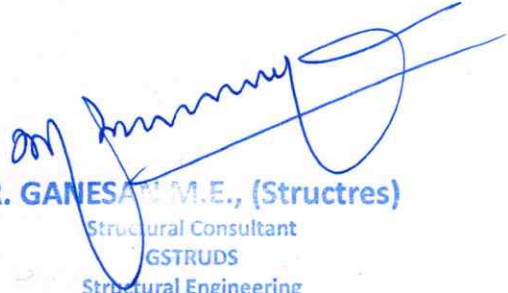
Using design aids, for M25, Fe 500, Table 3,

$$P_t = 0.811\%$$

$$A_t = \frac{0.811 \times 340 \times 702}{100} = 1935 \text{ mm}^2$$

$$\text{Provide } 4Y25 = 1964 \text{ mm}^2 > 1935 \text{ mm}^2$$

Hence Safe


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From interaction chart, SP16

$$\begin{aligned} M_{ux1}/f_{ck} b D^2 &= 0.11 \\ M_{ux1} &= 0.11 \times 230 \times 230 \times 600 \times 25 \\ &= 227.7 \text{ KN.m} \end{aligned}$$

Moment Capacity Along y Direction

$$\begin{aligned} (P_u/f_{ck} b D) &= (780000/25 \times 230 \times 600) \\ &= 0.23 \end{aligned}$$

$$\begin{aligned} p/f_{ck} &= 1.311/25 \\ &= 0.0524 \\ b'/D &= 32/230 \\ &= 0.14 \end{aligned}$$

From interaction chart, SP16

$$\begin{aligned} M_{uy1}/f_{ck} b D^2 &= 0.1 \\ M_{uy1} &= 0.1 \times 230 \times 230 \times 600 \times 25 \\ &= 207 \text{ KN.m} \end{aligned}$$

8 Check for Moment Capacity

$$(M_{ux}/M_{ux1})^{\alpha_n} + (M_{uy}/M_{uy1})^{\alpha_n} < 1$$

$$\begin{aligned} P_{uz} &= (0.45 f_{ck} A_c) + (0.75 f_y - 0.45 f_{ck}) A_{sc} \\ A_c &= 138000 \text{ mm}^2 \\ P_{uz} &= 2210.5238 \text{ KN} \\ P_u/P_{uz} &= 0.353 \\ \alpha_n &= 1.255 \end{aligned}$$

For $P_u/P_{uz} = 0.2$ to 0.8
 α_n varies from 1.0 to 2.0

$$\begin{aligned} (M_{ux}/M_{ux1})^{\alpha_n} + (M_{uy}/M_{uy1})^{\alpha_n} &= 0.238 \\ &0.238 < 1 \end{aligned}$$

O.K

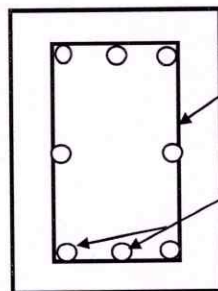
9 Calculation of Lateral Reinforcement

Spacing of ties

1. Least Lateral Dimensions of column = 230 mm
2. Sixteen times the least dia of Longi bar = 256 mm
3. 300mm = 300 mm

$$\text{Adopt Spacing} = 200 \text{ mm}$$

10 Details



Y8@200mm c/c

No of bars = 8 Nos

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Reinforcement at support section:

$$M_u/bd^2 \text{ (Hogging)} = \frac{793 \times 10^6}{340 \times (702)^2} = 4.73 \text{ N/mm}^2$$

Using design aids, for M25, Fe 500, Table 3,

$$P_t = 1.321 \% \quad P_c = 0.409 \%$$

$$A_t = \frac{1.321 \times 340 \times 702}{100} = 3153 \text{ mm}^2, \quad A_c = \frac{409 \times 340 \times 702}{100} = 976 \text{ mm}^2$$

Provide,

$$A_{st} : 7Y25 = 3437 \text{ mm}^2 > 3153 \text{ mm}^2$$

$$A_{sc} : 4Y25 = 1963 \text{ mm}^2 > 976 \text{ mm}^2$$

Hence Safe.

Design for Shear:

$$T_v \text{ Max} = \frac{V_u}{bd} = \frac{374 \times 1000}{340 \times 702} = 1.57 \text{ N/mm}^2$$

A_{st} provided 1030 mm^2

$$P_t = \frac{1964 \times 100}{340 \times 702} = 0.82 \%$$

Refer table, 61 of SP16, for M25 grade Concrete

$$T_c = 0.59 \text{ N/mm}^2$$

So, shear taken by stirrups ,

$$\frac{(T_v - T_c) \times b \times d}{1000} = \frac{(1.57 - 0.59) \times 340 \times 702}{1000} = 233.9 \text{ KN}$$

$$\text{Shear force per CM depth of beam} = \frac{233.9}{70.2} = 3.33 \text{ KN/cm depth of beam}$$

Refer table No. 62,

Provide 2 legged Y10 @150mm C/C

Size of beam (340 x 750)mm

Span reinforcement (Bottom) – 4Y25

Support reinforcement (Top) – 7Y25

Stirrups – Y10 @ 150mm C/C

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Design of slab

Four Edges Discontinuous

Fck	25 N/mm ²
Fy	500 N/mm ²
Dia of bar (Lx Direction)	12 mm
Dia of bar (Ly Direction)	10 mm
Clear cover	15 mm
Clear span Lx	5780 mm
Clear span Ly	7370 mm
Width of Beam	300 mm
Slab tk	175 mm
Floor Finish	45 mm
Weathering Coarse	5 mm
LIVE LOAD	4 KN/m ²
Length of slab (lx)	5934 mm
Length of slab (ly)	7519 mm
Dead Load	5.33 KN/m ²
LIVE LOAD	4 KN/m ²
FD D.L	7.995 KN/m ²
FD L.L	6 KN/m ²
ly/lx	1.2751 IT IS TWO WAY SLAB

**Bending Moment Coefficient for Rectangular Panels Supported on Four Sides
with Provision for Torsion at Corners (IS 456-2000 Table 26)**

	short span (-ve Mx) (+ve Mx (-ve My)	long span 0 (+ve My)
	0 0.0907	0.055781
support moment	Mx 0 KN.m My 0 KN.m	
span moment	Mx 44.692 KN.m My 27.489 KN.m	
Xu max/d	0.46	
Q	3.3402	
d required	115.67	The depth provide is sufficient
Effective depth shorter span	154	
Effective depth longer span	143	
Ast (+ ve Shorter span)	738.27 mm ²	
Ast (+ ve Longer span)	473.48 mm ²	
Ast (- ve Shorter span)	0 mm ²	
Ast (- ve Longer span)	0 mm ²	
Min Ast	210 mm ²	
SPAN REINFORCEMENT		
TO PROVIDE 12 mm DIA OF BAR @153 mm SPACING IN 5780 mm DIRECTION		
TO PROVIDE 10 mm DIA OF BAR @166 mm SPACING IN 7370 mm DIRECTION		
SUPPORT REINFORCEMENT		

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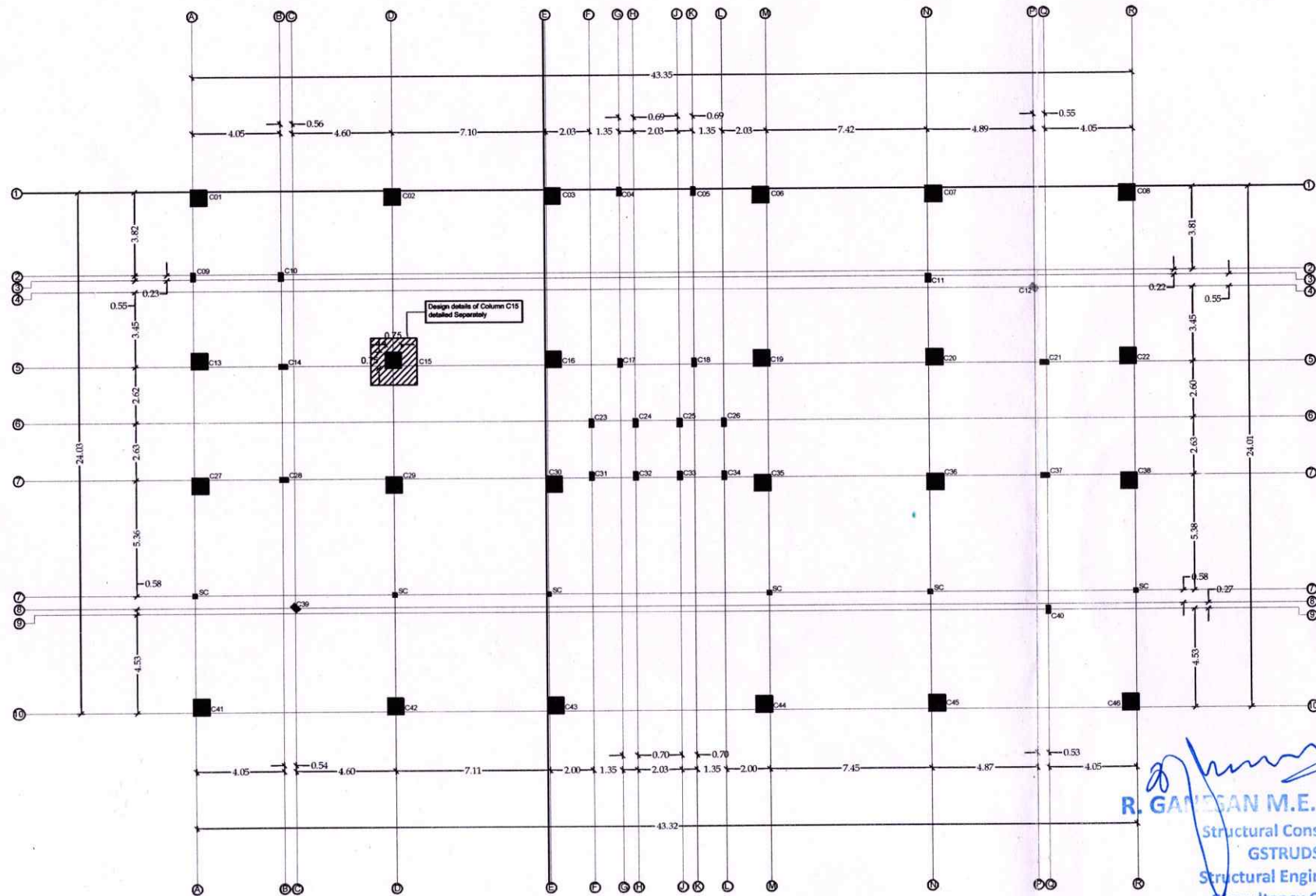
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Column & Grid Layout



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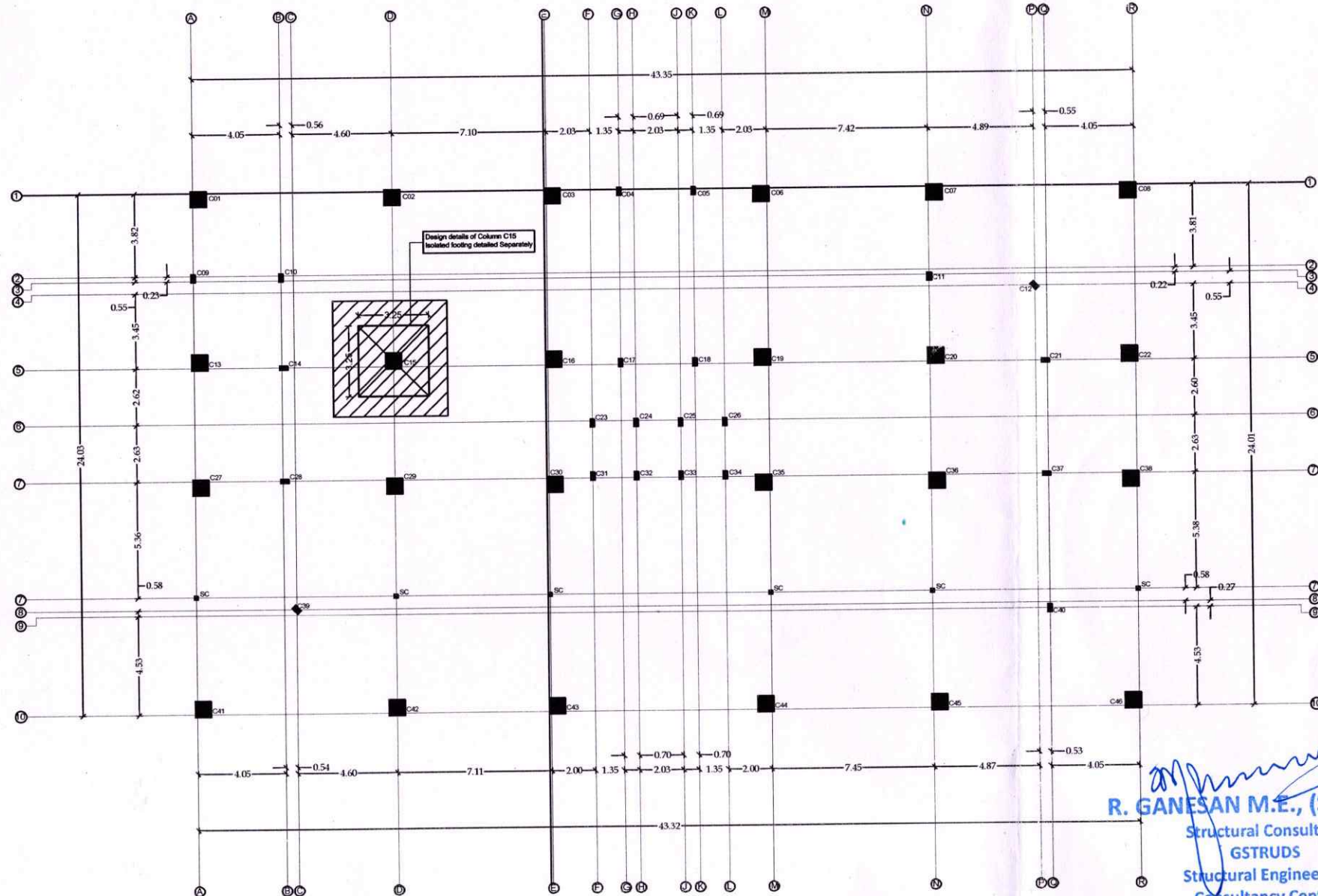
☒ - Stub Column

■ - Regular Column

▨ - Column to be terminated at Basement Floor - 1

▩ - Column to be terminated at Basement Floor - 2

Foundation Layout



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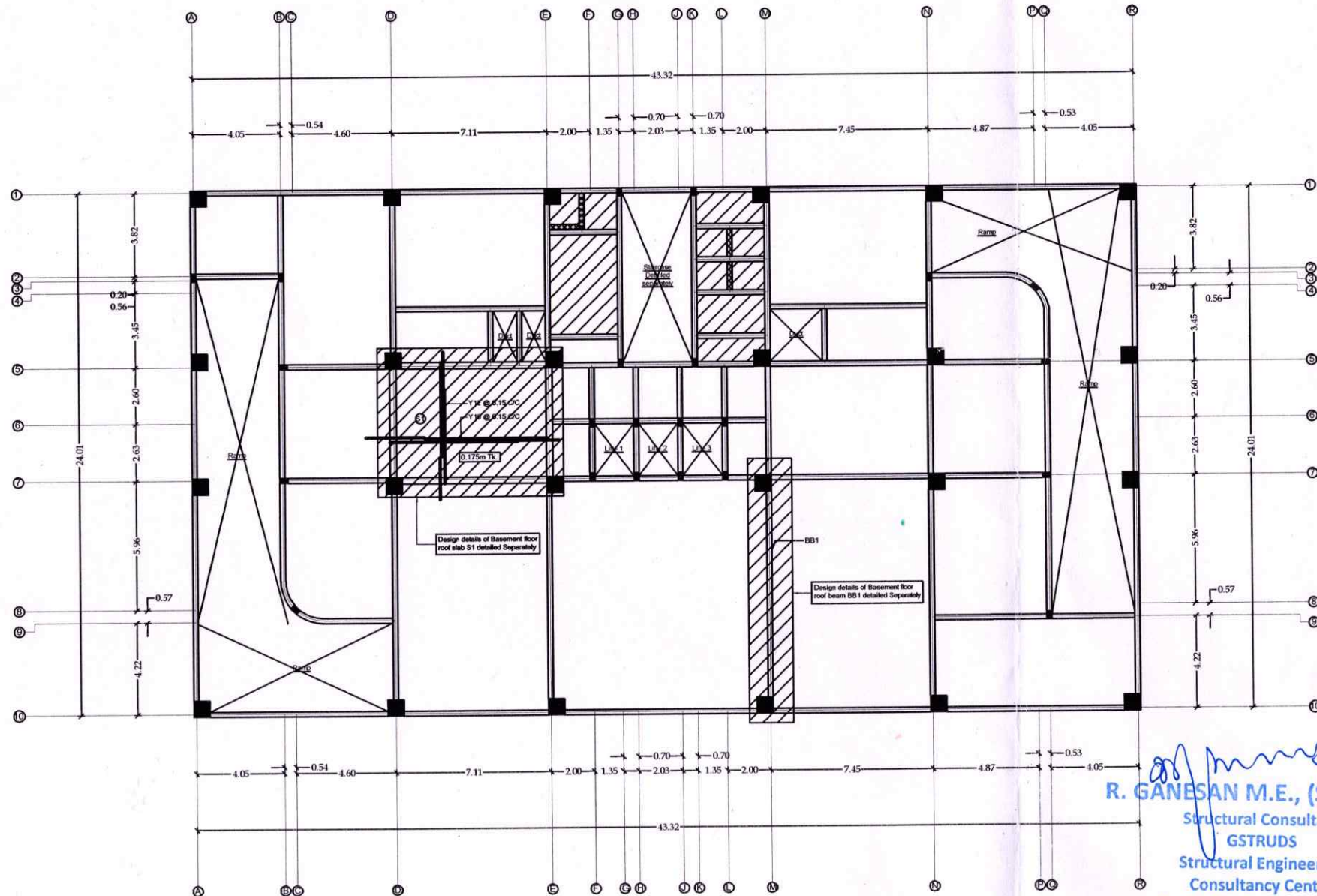
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Basement Floor - 2 Roof Beam Layout.



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I.P.A REG NO: SE/GP/TLPA/MAY2019/029

■ - Regular Column

■ - Column to be terminated at Basement Floor - 1

■ - Column to be terminated at Basement Floor - 2

⊠ - Stub Column

■ - Sunken by beam bottom

DIRECTORATE OF TOWN AND COUNTRY PLANNING
(Government of Tamil Nadu)
(807 Anna Salai, Chennai 600 002)

TIRUCHIRAPPALLI LOCAL PLANNING AUTHORITY
(Kajamalai Main road, Kajamalai, Tiruchy 620 023)

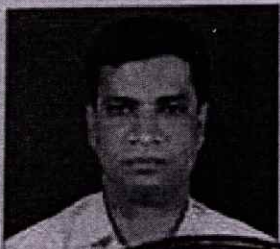
PROFESSIONAL REGISTRATION CERTIFICATE

This is to certify that Thiru R.GANESAN has enrolled as **STRUCTURAL ENGINEER GRADE-I** with this office who has the qualification of M.E., in Structural Engineering and experience in the relevant field for 29 years.

He has been given the Registration No. SE/Gr.I/TLPA/May2019/029 on 08.05.2019.

He shall be required to comply with the duties and responsibilities prescribed by the Government of Tamil Nadu in Part V, "Registration of Professionals", Tamil Nadu Combined Development and Building Rules 2019, approved vide G.O (Ms) No.18 MAWS (MA1) Department dated 4.2.2019.

This Registration is valid up to 07.05.2024

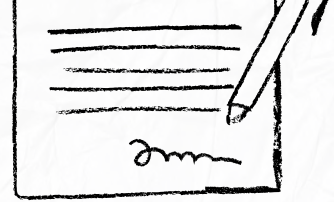


[Signature]
Member Secretary,

Tiruchirappalli Local Planning Authority,
Tiruchirappalli

[Stamp]
8.5.19





our services doesn't just end there



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Property Development & Approvals

Building plan approvals, construction, layout and sub-division approvals, zone conversion, and occupancy certification.



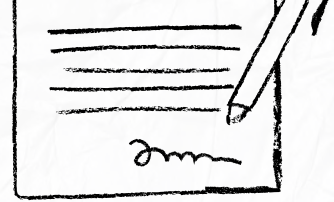
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Escrow Services, Rentals, Litigation Solutions, Property Valuation and Property Management



Compliance & Special Services

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with smart tools



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Zoning & Land Use Analysis

Land Use Zone Finder, CRZ Zone Check, Aquifer Zone Check, CBA Check, EWS Check, Road Width Check, Proposed Road Widening Check, FSI Calculator



Property Documentation & Workflow Tools

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