

LORDS ENGINEERING STRUCTURAL

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STRUCTURAL STABILITY DESIGN BASIS CALCULATION REPORT

FOR

CONSTRUCTION OF

STILT FLOOR + 5 FLOORS RESIDENTIAL BUILDING

BLOCK - A & BLOCK - B (HEIGHT 18.30M) WITH

15 DWELLING UNITS (AVAILING PREMIUM FSI),

AT BLOCK NO: 12 & PLOT NO. 81, VGP NAGAR,

VIOLET APARTMENTS STREET AND VELLALAR STREET,

MOGAPPAIR WEST, CHENNAI - 600037,

COMPRISED IN OLD S.NO:

245/2&3, T.S.NO: 29/2 & 3, 65/2 & 3,

BLOCK NO.36, WARD - H OF MOGAPPAIR VILLAGE,

AMBATTUR TALUK, WITHIN THE LIMITS OF

GREATER CHENNAI CORPORATION.

CLIENT: M/s. NEXA INFRA PROJECT.

31-07-2025

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STRUCTURAL STABILITY CERTIFICATE

I Hereby Certify That the Proposed Residential Building at Construction of Stilt Floor + 5 Floors Residential Building Block - A & Block - B (Height 18.30m) With 15 Dwelling Units (Availing Premium FSI), At Block No: 12 & Plot No. 81, VGP Nagar, Violet Apartments Street And Vellalar Street, Mogappair West, Chennai - 600037, Comprised In Old S.No: 245/2&3, T.S.No: 29/2 & 3, 65/2 & 3, Block No.36, Ward - H of Mogappair Village, Ambattur Taluk, Within The Limits Of Greater Chennai Corporation.

Designed and Checked for Dead Load and Live Load and Also Resist Earthquake Forces and Found Safe. Reference: BOOSHNAM ASSOCIATES/ JOB NO: BAG/M/s. NEXA INFRA PROJECTS/D-1738/25-26.

The following assumptions and basic values are considered for the design and analysis of the structure under the title of the project.

- 1. The least dimension of the column for the Stilt floor is 300 mm, and for other columns is 230mm.**
- 2. The grade of concrete for structural elements is M30.**
- 3. The Safe Load Carrying Capacity of pile is 55 MT as per the soil report.**
- 4. The proposed type of foundation is Pile Foundation.**
- 5. The length of pile as per soil report is 20.20 m below existing ground level.**
- 6. The design, analysis, detailing and drafting is carried out using the various code of practice namely and as per IS 875 for Loads and loading combinations, IS 1786 for High Tensile Reinforcement bar, IS 456 for Practice of plain and reinforced concrete and IS 1893 for Seismic design. Etc.**
- 7. The Registered Construction Project Engineer at site shall take necessary precautions in adhering to the relevant Code provisions while executing the above work.**

NOTE: The structural design is prepared based on the copy of Approval Plan of the building. Any change/alteration/ addition/ modification of the building plan in further Approval or during construction hereafter, it should be brought to the knowledge of structural engineer and work shall be carried out with new structural design report by the engineer.

STRUCTURAL DESIGN ANALYSIS FOR PROPOSED BUILDING

Name of work:

Construction of Stilt Floor + 5 Floors Residential Building Block - A & Block - B (Height 18.30m) With 15 Dwelling Units (Availing Premium FSI), At Block No: 12 & Plot No. 81, VGP Nagar, Violet Apartments Street And Vellalar Street, Mogappair West, Chennai - 600037, Comprised In Old S.No: 245/2&3, T.S.No: 29/2 & 3, 65/2 & 3, Block No.36, Ward - H of Mogappair Village, Ambattur Taluk, Within The Limits Of Greater Chennai Corporation.

Preambles:

1. I hereby certify that the structural design is done by **limit state method, as per relevant sections of IS 456.**
2. I hereby certify that the structural design sheet is done for critical column, beam, slab and foundation for the proposed building.
3. The usage of the building is **Block-A (Stilt+05) & Block-B (Stilt+05) Floors Residential Building.**
4. The building consists of **For Proposed Construction of the Block-A (Stilt+05) & Block-B (Stilt+05) Floors Residential Building.**
5. The superstructure is built on **230 mm thick outer walls and 115 mm thick inner walls.**
6. The structural design includes the **earthquake Criteria as per the IS 1893.**

IS Code:

IS 456 for concrete.

IS 875 for design load.

IS 1786 for steel reinforcement.

IS1893 for earthquake design.

IS13920 for ductile design.

GENERAL NOTES ON STRUCTURAL DESIGN

- **General:**

Design Basis

Design Of The Building Is Carried Out By RCC Frame Analysis Using Etabs Software And Critical Members Are Checked And Designed By RCDC software output As Enclosed Below.

- **Codes and Standards**

All Structural design is carried out confirming to the provisions in National Building Code of India and other relevant Indian Codes and Standards.

IS Code used for design purposes were:

IS 456:2000 for Concrete

IS 875:2007 for Design Load

IS 1786: 2008 for Steel Reinforcement

IS 1893:2002 for Earthquake design

- **Concrete:**

The concrete shall be in grades designated as per Table 5 of IS 456-2000. Recommended grades for the different members is as follows:

Foundation	M30
Columns	M30
Roof beams and slab	M30


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- **Material, Workmanship, Inspection and testing:**

The Proposed RCC Structure will consist of cement concrete and reinforcement as the main material used for construction of the structure. The specifications for these materials are discussed below.

- **Design methods:**

General Design and Detailing of concrete members / elements are done confirming to the provisions of IS. 456 and other relevant IS codes. Limit State Method is followed for the design.

Seismic Zone III load is taken into account for the analysis. The predominant direction of vibration is horizontal. Relevant combination of forces has been taken into account.

- **Minimum Cover:**

Slab	20mm
Beam	25mm
Columns	40mm
Foundation	50mm


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PILECAP DESIGN CALCULATIONS

Definitions:

- | | | |
|------------------|---|--|
| 1. α | = | Coefficient of Thermal Expansion |
| 2. ϵ_1 | = | Strain at level considered, Calculated ignoring the stiffening of the concrete in tension zone |
| 3. ϵ_m | = | Average steel strain at level considered |
| 4. p_{act} | = | Percentage steel provided |
| 5. p_{crit} | = | Percentage steel critical as per code |
| 6. A_1 | = | Area of Base for Load Transfer |
| 7. A_2 | = | Area of Bearing under column |
| 8. a_{cr} | = | Distance from the point considered to the surface of the nearest longitudinal bar |
| 9. A_{sfrPrv} | = | Area of face reinforcement provided |
| 10. A_{sfrReq} | = | Area of face reinforcement required |
| 11. A_{stPrv} | = | Area of tensile reinforcement provided |
| 12. A_{stReq} | = | Area of tensile reinforcement required |
| 13. A_{svPrv} | = | Area of shear reinforcement provided |
| 14. A_{svReq} | = | Area of shear reinforcement required |
| 15. A_v | = | Location of section of shear-check from Pile Center |
| 16. B_{eff} | = | Effective Width for design for bending and shear |
| 17. B_{effsfr} | = | Effective Width for design for Face Reinforcement |
| 18. B_{Mux} | = | Factored Bending Moment for pile-cap along column D |
| 19. B_{Muy} | = | Factored Bending Moment for pile-cap along column B |
| 20. D | = | Depth of Pilecap |
| 21. D_{eff} | = | Effective Depth of Pilecap |
| 22. D_{fCol} | = | Distance of Pile center to face of column |
| 23. E_c | = | Modulus of elasticity of concrete |
| 24. E_s | = | Modulus of elasticity of steel |
| 25. F_{st} | = | Stress in steel |
| 26. M_x | = | Bending Moment in column along Column D |
| 27. M_y | = | Bending Moment in column along Column B |


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28. P	=	Axial load in pile due to Ptotal
29. Pcomb	=	Axial load in column for a load combination
30. Ppile	=	Axial Load on pile
31. Ptotal	=	Total vertical load on pile-cap for a load combination
32. Pmx	=	Axial load on pile due to moment Mx
33. Pmy	=	Axial load on pile due to moment My
34. sp	=	Spacing Between bars at outer most layer
35. Tc	=	Design Shear Strength of Concrete
36. Tce	=	Enhanced Shear Strength of concrete
37. Temp1	=	Peak Hydration temperature
38. Temp2	=	Seasonal Temperature Variations
39. Tv	=	Nominal shear stress
40. Vu	=	Design shear force
41. Vus	=	Design shear force for stirrups
42. Wcr	=	Surface Crack Width

Code References:

IS 456

1. P _{tmax}	:	clause 26.5.1.1
2. P _{tmin}	:	clause 26.5.2.1
3. P _t	:	clause 38
4. T _c	:	clause 40.2.1
5. T _{cmax}	:	clause 40.2.3
6. A _{svReq}	:	clause 40.4
7. Min Shear Reinf	:	clause 26.5.1.6
8. Max Stirrup Spacing	:	clause 26.5.1.5
9. One Way Shear Criteria	:	clause 34.2.4.2
10. Load transfer	:	clause 34.4
11. P _{tnominal}	:	clause 34.5.2
12. crack width calculation	:	Annex-F
13. cracking	:	clause. 35.3.2

IS 2911 Part-1 Section 2

1. Pile capacity check	:	clause 5.10
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BS 8007 (For Early / Initial Thermal Cracking)

1. Surface Zone for suspended slab	:	Figure A.1
2. Surface Zone for ground slab	:	Figure A.2
3. Factors for the calculation of minimum reinforcement	:	Table A.1

Design Code : IS 456 : 2000 + IS 13920 : 2016
 Pilecap No : PC2
 Column No : C1 (300mm x 900mm)
 Member Ref. No : 159

Concrete Grade : M30
 Steel Grade : Fe550
 Clear Cover : 75 mm
 Top of pile-cap below ground : 1.0 m

Density of Soil = 18 kN/cum
 Founding Depth = 4 m
 Pile Capacity in Compression = 750 kN
 Pile Capacity in Tension = 780 kN
 Pile Capacity in Shear = 70 kN
 Pile Capacity Reduction = 0 %
 Pile Overloading = 10 %
 Pile Group Overloading = 10 %
 Pile Capacity Increase for EQ = 25 %
 Pile Capacity Increase for Wind = 25 %
 Live Load Reduction = 0 %

Consider Capacity Design : No
 Consider Overburden Pressure : No

No. of Piles = 4
 Pile Diameter = 600 mm
 Pilecap Offset = 150 mm
 Pile Spacing = 3.0 x Ø
 Pilecap Size = 2.40 x 2.40 m
 Pilecap Depth = 1000 mm
 Pile-cap Wt. = 21.094 kN

For design, moments along shorter direction of pile cap has been ignored

Check for Maximum Compressive Load on One Pile:

Critical Analysis Load : 302
 Combination
 Critical Load Combination : [2] : (LOAD 9: DL) +0.8 (LOAD 10: LL) +0.8 (LOAD 1: EQ+X)
 Pcomb = 1048.05 kN

$$\begin{aligned}
 P_{total} &= P_{comb} + \text{Pilecap Wt.} \\
 &= 1069.14 \quad \text{kN} \\
 M_x &= -24.17 \quad \text{kNm} \\
 M_y &= 0.8 \quad \text{kNm} \\
 P &= P_{total} / \text{No. of Piles} \\
 &= 534.57 \quad \text{kN} \\
 P_{mx} &= 21.484 \quad \text{kN} \\
 P_{my} &= 0 \quad \text{kN}
 \end{aligned}$$

$$\begin{aligned}
 \text{Maximum Compressive load on pile} &= 556.06 \quad \text{kN} \\
 \text{Allowable Compressive load on pile} &= 600 \times 1.25 \times 1.1 \\
 &= 825 \quad \text{kN}
 \end{aligned}$$

Check for Maximum Compressive Load on Pile Group:

$$\begin{aligned}
 \text{Critical Analysis Load Combination} &: 301 \\
 \text{Critical Load Combination} &: [1] : (\text{LOAD 9: DL}) + (\text{LOAD 10: LL}) \\
 P_{comb} &= 1046.66 \quad \text{kN} \\
 P_{total} &= P_{comb} + \text{Pilecap Wt.} \\
 &= 1067.75 \quad \text{kN} \\
 M_x &= 4.89 \quad \text{kNm} \\
 M_y &= 0.2 \quad \text{kNm}
 \end{aligned}$$

$$\begin{aligned}
 \text{Maximum Compressive load on pile group} &= 1067.76 \quad \text{kN} \\
 \text{Allowable Compressive load on pile group} &= 2 \times 600 \times 1.1 \\
 &= 1320 \quad \text{kN}
 \end{aligned}$$

Check for Maximum shear on Pile Group:

$$\begin{aligned}
 \text{Critical Analysis Load Combination} &: 307 \\
 \text{Critical Load Combination} &: [7] : (\text{LOAD 9: DL}) + (\text{LOAD 2: EQ-X}) \\
 P_{comb} &= 821.46 \quad \text{kN} \\
 P_{total} &= P_{comb} + \text{Pilecap Wt.} \\
 &= 842.55 \quad \text{kN} \\
 M_x &= 39.88 \quad \text{kNm} \\
 M_y &= -0.74 \quad \text{kNm} \\
 V_x &= -2.05 \quad \text{kNm} \\
 V_y &= -28.68 \quad \text{kNm} \\
 \text{Maximum shear on pile group} &= \sqrt{(-2.05)^2 + (-28.68)^2} \\
 &= 28.75 \quad \text{kN}
 \end{aligned}$$

$$\begin{aligned}\text{Shear capacity of pile group} &= 2 \times 100 \times 1 \times 1.25 \\ &= 250 \quad \text{kN}\end{aligned}$$

Check for Tensile Load on One Pile:

No Tensile load in pile group.

Check for Maximum Tensile Load on Pile Group:

No Tensile load in pile group.

Design for Bending:

Bottom Reinforcement Along Column-D

$$\begin{aligned}\text{Critical Analysis Load} &: 401 \\ \text{Combination} & \\ \text{Critical Load Combination} &: [74] : 1.5 (\text{LOAD 9: DL}) + 1.5 (\text{LOAD 10: LL}) \\ P_{\text{comb}} &= 1569.99 \quad \text{kN} \\ P_{\text{total}} &= P_{\text{comb}} + \text{Pilecap Wt.} \\ &= 1601.631 \quad \text{kN} \\ M_x &= 7.33 \quad \text{kNm} \\ M_y &= 0.3 \quad \text{kNm} \\ P_{\text{pile}} &= \text{Max Load on pile} \\ &= 807.33 \quad \text{kN} \\ \\ D_{\text{eff}} &= 540 \quad \text{mm} \\ B_{\text{eff}} &= 750 \quad \text{mm} \\ D_{\text{fCol}} &= 0.34 \quad \text{m} \\ B_{\text{Mux}} &= P_{\text{pile}} \times D_{\text{fCol}} \\ &= 272.48 \quad \text{kNm} \\ P_{\text{tReq}} &= 0.27 \quad \% \\ A_{\text{stReq}} (\text{BM}) &= 1481 \quad \text{sqmm/m} \\ A_{\text{stPrv}} &= \text{T16 @ 150 C/C} \\ &= 1608.48 \quad \text{sqmm/m}\end{aligned}$$

Top Reinforcement Along Column-D

There is no Tensile Force, hence Minimum Percentage of steel will be provided.

$$\begin{aligned}D &= 1150 \quad \text{mm} \\ A_{\text{stReq}} (\text{BM}) &= \text{Min Pt for Top Reinforcement} \times D \times 1000/100 \\ &= 0.06 \times 1150 \times 1000/100 \\ &= 690 \quad \text{sqmm/m} \\ A_{\text{stPrv}} &= \text{T12 @ 150 C/C} \\ &= 392.7 \quad \text{sqmm/m}\end{aligned}$$

Bottom Reinforcement Along Column-B

There is no Compressive Force, hence Minimum Percentage of steel will be provided.

$$\begin{aligned}
 D &= 1150 \text{ mm} \\
 A_{stReq} \text{ (BM)} &= \text{Min Pt for Bottom Reinforcement} \times D \times 1000/100 \\
 &= 0.2 \times 1150 \times 1000/100 \\
 &= 2300 \text{ sqmm/m} \\
 A_{stPrv} &= T16 @ 150 \text{ C/C} \\
 &= 1340.4 \text{ sqmm/m}
 \end{aligned}$$

Top Reinforcement Along Column-B

There is no Tensile Force, hence Minimum Percentage of steel will be provided.

$$\begin{aligned}
 D &= 1150 \text{ mm} \\
 A_{stReq} \text{ (BM)} &= \text{Min Pt for Top Reinforcement} \times D \times 1000/100 \\
 &= 0.06 \times 1150 \times 1000/100 \\
 &= 690 \text{ sqmm/m} \\
 A_{stPrv} &= T12 @ 200 \text{ C/C} \\
 &= 392.7 \text{ sqmm/m}
 \end{aligned}$$

Design for One Way Shear:

Along Column-D (Compression Case)

$$\begin{aligned}
 \text{Critical Analysis Load Combination} &: 401 \\
 \text{Critical Load Combination} &: [74] : 1.5 (\text{LOAD 9: DL}) + 1.5 (\text{LOAD 10: LL}) \\
 P_{comb} &= 1569.99 \text{ kN} \\
 P_{total} &= P_{comb} + \text{Pile cap Wt.} \\
 &= 1601.63 \text{ kN} \\
 M_x &= 7.33 \text{ kNm} \\
 M_y &= 0.3 \text{ kNm} \\
 P_{pile} &= \text{Max Load on pile} \\
 &= 807.3347 \text{ kN}
 \end{aligned}$$

Location of critical section is at $d/2$ from face of column

$$\begin{aligned}
 \text{Section Location from column center} &= 495 \text{ mm}
 \end{aligned}$$

Data for Piles

Pile No	Load (kN)	% covered	Shear (kN)
P1	600	40	460
P2	600	40	460
P3	600	40	460
P4	600	40	460

Design Shear Force (V_u)	=	Max. of (Shear due to P1, P2)
	=	524.77 kN
D_{eff}	=	540 mm
B_{eff}	=	750 mm
T_v	=	$V_u / (B_{eff} \times D_{eff})$
	=	1.3 N/sqmm
T_c	=	0.384 N/sqmm
A_v	=	67.5 mm
Shear enhancement factor	=	$2 \times D_{eff} / A_v$
	=	16
Enhanced shear strength (T_{ce})	=	3.5 N/sqmm
T_v	<	T_{ce} , Hence Shear Reinforcement is not required

Along Column-D (Tension Case)

All Load Combination having Compressive Force. Thus, One way Shear is not applicable for Tensile Force.

Along Column-B (Compression Case)

One way shear check do not applicable for 2 pile pile-cap design

Along Column-B (Tension Case)

One way shear check do not applicable for 2 pile pile-cap design

Design of Face Reinforcement:

$A_{sfr\ Req}$	=	$SFR \% \times D \times B_{effsfr}$
	=	$0.05 \times 600 \times 500 / 100$
	=	150 sqmm
$A_{sfr\ Prv}$	=	2-T10
	=	157 sqmm

Check for Load Transfer from Column to PileCap

Critical Analysis Load Combination	=	401
Critical Load Combination	:	[74] : 1.5 (LOAD 9: DL) + 1.5 (LOAD 10: LL)
P	=	1569.99 kN
A_2	=	0.14 sqm
A_1	=	1.41 sqm
Base Area	=	1.41 sqm
A_1	<	Base Area
Modification Factor	=	$\text{SquareRoot}(A_1/A_2) \leq 2$
$\text{SquareRoot}(A_1/A_2)$	=	3.23
Thus, Modification Factor	=	2

Concrete Bearing Capacity = $0.45 \times F_{ck} \times \text{Modification Factor} \times \text{Column Area}$
= 3645 kN
Concrete Bearing Capacity > P, Hence Safe.



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COLUMN DESIGN CALCULATIONS

Definitions Of Terms:

All forces in units kN and m

All reinforcement details like area, spacing are mm

Grade Of steel for 6 mm dia. bars is Fe250. It is irrespective of the grade of steel defined by user in column design.

Neutral axis angle for resultant design moment is with respect to local major axis.

1 β	=	Stiffness proportion factor at joint (column stiffness/sum of stiffness of all members connected at joint)
2 Δu	=	Elastically computed first order lateral deflection. (Relative deflections)
3 ϵl	=	Strain at level considered, Calculated ignoring the stiffening of the concrete in tension zone
4 ϵm	=	Average steel strain at level considered
5 a_{cr}	=	Distance from the point considered to the surface of the nearest longitudinal bar
6 A_g	=	Gross area of the column cross section
7 A_{eff}	=	Effective area of column / wall considered for shear check in sqmm
8 A_k	=	Area of confined concrete core
9 A_{sh}	=	Area of link cross section
10 b	=	Effective Width of Column in mm
11 b_{eff}	=	Effective Width of Column in mm
12 B	=	Width / Smaller Dimension of Column in mm
13 d	=	Effective Depth of Column in mm
14 d_{eff}	=	Effective Depth of Column in mm
15 D	=	Depth / Larger Dimension of Column OR Diameter of Circular Column in mm
16 D_k	=	Diameter Of core measured to the outside of circular link
17 E_c	=	Modulus of elasticity of concrete
18 E_s	=	Modulus of elasticity of steel
19 F_{cPerm}	=	Permissible Stress in Concrete required in N/ (sqmm)
20 F_{st}	=	Stress in steel
21 F_{stPerm}	=	Permissible Stress in Steel required in N/ (sqmm)



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22 f_{ck}	=	Characteristic compressive strength of concrete cube in N/sqmm
23 F_y	=	Yield Stress Of Steel in N/sqmm
24 h	=	Longer dimension of rectangular link measured to its outer face
25 H_u	=	Total lateral force acting within the story (Story shear)
26 H_s	=	Height of the story (Floor height)
27 k	=	Reduction factor for slenderness moments
28 M_{ax}	=	Additional moment due to slenderness about major axis (Along D)
29 M_{ay}	=	Additional moment due to slenderness about minor axis (Along B)
30 M_{minx}	=	Moment due to minimum eccentricity along D
31 M_{miny}	=	Moment due to minimum eccentricity along B
32 M_{uv}	=	Moment capacity of web portion of wall as per clause 9.4.2 and Annex A of IS 13920 - 2016
33 M_{ux}	=	Factored moment Along D (Moment About Major Axis)
34 M_{uy}	=	Factored moment Along B (Moment About Minor Axis)
35 M_{Cap}	=	Moment capacity of section for NA angle at design P_u
36 M_{Res}	=	Resultant design moment at angle to local major axis
37 P_b	=	Axial capacity of column along B as defined in 39.7.1.1
38 P_d	=	Axial capacity of column along D as defined in 39.7.1.1
39 P_u	=	Factored axial force
40 P_{uz}	=	Axial load on column as defined in 39.6
41 P_{u_Total}	=	Sum of Axial loads on all column in the story (Gravity Load)
42 Q	=	Stability Index (factor for checking sway/ non sway condition for a given story)
43 s	=	Link Spacing
44 Shear Strength Enhancement Factor	=	Multiplying factor for shear strength of concrete as per 40.2.2
45 V_{ur}	=	Factored resultant shear force acting on the column
46 V_{ux}	=	Factored shear force Along B
47 V_{uy}	=	Factored shear force Along D
48 W_{cr}	=	Surface Crack Width
49 W_{crPerm}	=	Permissible Crack Width required in mm
50 β	=	It is a Neutral Axis angle corresponding to load angle to find out M_{Cap}

Code References:**IS 456**

	ELEMENT	CLAUSE / table
1	Max area of reinforcement	26.5.3.1-a & b
2	Min area of reinforcement	26.5.3.1-a & b
3	Min number of bars	26.5.3.1-c
4	Minimum Eccentricity Calc	25.4 & 39.2
5	Effective Length	25.2
6	Slenderness Moments	25.3 & 39.7
7	Design for axial loads	39.3
8	Design for axial loads And uniaxial bending	39.5
9	Design for axial loads And Biaxial bending	39.6
10	Design of horizontal links	26.5.3.2
11	Design shear strength	40.2
12	Stiffness Proportion Factor, β	E-1
13	Stability(Index, Q)	E -2
14	Crack width calculation	3.8
15	Multiplying factor to Beam Stiffness for effective length calculation	SP 24 1983 APPENDIX D

IS 13920 - 2016

	ELEMENT	CLAUSE / table
1	Spacing of special confining reinforcement	10.4 and 7.6
2	C/s area of special confining reinforcement	7.6.1
3	Applicability of boundary element	10.4.1
4	Muv-Moment Capacity of Web	Annex
5	Additional Compressive Force in BE	10.4.2
6	Check for BE in tension and compression	10.4.2.1 and 10.4.3
7	Shear include due to Beam	7.5
8	Minimum Flexural Strength of Column	7.2
9	Shear Check at Column Joint	9.1
10	Length of wall to thickness ratio	10.1.3
11	Type of wall & Minimum reinforcement	10.1.4
12	Largest diameter of longitudinal steel bar	10.1.8
13	Shear reinforcement in RC wall	10.2.3
14	Special confinement reinforcement in Boundary Element	10.4.4
15	Minimum vertical reinforcement across horizontal construction joint	10.7

Sway Calculation (Stability Index)

For Global-X Direction

Level	Load Name	Storey Height	Gravity Load P	Relative Displacements	Storey Shear	Stability Index	Sway Condition
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		(m)	(kN)	(mm)	(kN)		
		A	B	C	D	B x C / (A x D)	
FOUNDATION to GRADE BEAM	EQ+X	1	15492.026	0.313	1139.527	0.004	Non Sway
GRADE BEAM to GFR	EQ+X	3	15027.2	3.121	1138.902	0.014	Non Sway
GFR to FFR	EQ+X	3	12520.649	5.207	1118.162	0.019	Non Sway
FFR to SFR	EQ+X	3	10057.709	6.003	1054.932	0.019	Non Sway
SFR to TFR	EQ+X	3	7594.768	5.806	925.891	0.016	Non Sway
TFR to 4FR	EQ+X	3	5131.827	5.003	707.812	0.012	Non Sway
4FR to 5FR	EQ+X	3	2668.886	4.024	377.467	0.009	Non Sway
5FR to HR	EQ+X	2.5	205.95	74189743848.581	65.231	93694455.086	Sway

For Global-Y Direction

Level	Load Name	Storey Height (m)	Gravity Load P (kN)	Relative Displacements (mm)	Storey Shear (kN)	Stability Index	Sway Condition
		A	B	C	D	B x C / (A x D)	
FOUNDATION to GRADE BEAM	EQ+Y	1	15492.026	0.613	1179.326	0.008	Non Sway
GRADE BEAM to GFR	EQ+Y	3	15027.2	5.887	1178.679	0.025	Non Sway
GFR to FFR	EQ+Y	3	12520.649	8.269	1157.215	0.03	Non Sway
FFR to SFR	EQ+Y	3	10057.709	8.333	1091.777	0.026	Non Sway
SFR to TFR	EQ+Y	3	7594.768	7.427	958.229	0.02	Non Sway
TFR to 4FR	EQ+Y	3	5131.827	5.796	732.533	0.014	Non Sway
4FR to 5FR	EQ+Y	3	2668.886	3.757	390.651	0.009	Non Sway
5FR to HR	EQ+Y	2.5	205.95	1534422225453.62	67.509	1872429192.299	Sway

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	FOUNDATION To GRADE BEAM	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	300	mm
Wall D	=	900	mm
Clear Cover	=	40	mm
Clear Floor Height @ B	=	550	mm
Clear Floor Height @ D	=	550	mm

No Of Floors = 1
 No Of Walls In Group = 1
 Wall Type : UnBraced
 Minimum eccentricity check : One Axis at a Time
 Code defined D/B ratio : 4
 D/B Ratio : 4.07 $\geq$ 4 Hence, Design as Wall

Flexural Design (Analysis Forces)

Analysis Reference No. = C1
 Load Combination = [29] : 1.5 (DL) -1.5 (EQ-X)
 Critical Location = Bottom Joint
 Pu = 2307.35 kN
 Mux = 1180.55 kNm
 Muy = -24.27 kNm
 Vux = -27.19 kN
 Vuy = 279.03 kN

Effective Length Calculation

Calculation Along Major Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	4972.905	No Beam	No Beam	-	-	1
Top	4972.905	No Beam	11790 x 230 x 450	-	16.228	0.998

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Major Axis = 1

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	300.7	No Beam	No Beam	-	-	1
Top	300.7	No Beam	10200 x 230 x 450	-	18.757	0.955

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Minor axis = 0.98

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in Y-direction

Minimum Eccentricity Along B :

$$\begin{aligned}\text{Minimum Eccentricity} &= \text{Unsupported Length} / 500 + B / 30 \\ &= 11.1 \text{ mm} \\ M_{\text{miny}} &= P_u \times \text{Minimum Eccentricity} \\ &= 46.15 \text{ kNm}\end{aligned}$$

Slenderness Check

$$\begin{aligned}\text{Max Slenderness Ratio}(L/B) &= 1.83 \\ &< 60 \quad (\text{Hence Ok})\end{aligned}$$

Column Is Unbraced Along D

Slenderness Check Along D:

$$\begin{aligned}\text{Effective Length Factor} &= 1 \\ \text{Slenderness Ratio} &= \text{Effective Length} / D \\ &= 0.45, \text{ Wall not Slender Along D}\end{aligned}$$

Column Is Unbraced Along B

Slenderness Check Along B:

$$\begin{aligned}\text{Effective Length Factor} &= 0.98 \\ \text{Slenderness Ratio} &= \text{Effective Length} / B \\ &= 1.8, \text{ Wall Not Slender Along B}\end{aligned}$$

Calculation of Design Moment

Direction	M _{analysis}	M _{min} (Abs)	M _{design}	M _{sldnx} (Abs)	M _{design-final}
	A	B	C	E	F
Major Axis - M _{ux}	1180.55	---	1180.55	0	1180.55
Minor Axis - M _{uy}	-24.27	46.15	-46.15	0	-46.15

Where

- A = Moments directly from analysis
- B = Moments due to minimum eccentricity
- C = Maximum of analysis moment and min. eccentricity = Max (A,B)
- E = Moment due to slenderness effect
- F = Final design Moment = Max(C- Top Bottom , D- Top Bottom) + E

Final Critical Design Forces

$$\begin{aligned}P_u &= 2307.35 \text{ kN} \\ M_{ux} &= 1180.55 \text{ kNm} \\ M_{uy} &= -46.15 \text{ kNm}\end{aligned}$$

Resultant Moment (Combined Action)**Moment Capacity Check**

Pt Calculated	=	0.89	
Reinforcement Provided	=	14-T25 + 12-T20 + 8-T12	
Load Angle	=	$\tan^{-1}(M_{uy}/M_{ux})$	
	=	2.24	deg
MRes	=	1181.46	kNm
MCap	=	1241.82	kNm
Capacity Ratio	=	MRes/ MCap	
	=	0.95 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	7-T16	4-T12	7-T16
Ast provided	1407.43	452.39	1407.43
Pt as % of entire wall	0.38 %	0.12 %	0.38 %
Pt as % of zone	1.56 %	0.24 %	1.56 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load Combination	[26] : 1.5 (DL) + 1.5 (EQ+X)	[32] : 1.5 (DL) - 1.5 (EQ+Y)
Design shear force, Vu (kN)	279.0333	-90.4618
Design shear stress, Tv (N/sqmm)	$V_u / (B \times 0.8 \times D)$	$V_u / (B \times 0.8 \times D)$
	0.953	0.309
Pt (%)	0.446	0.446
Height of Wall, Hw (mm)	550	550
Length of Wall, Lw (mm)	1220	300
Hw/Lw	0.4508	1.8333
	<= 1	> 1
Thus Shear Strength, Tc	$3.0 - (Hw/Lw) \times K1 \times \text{SquareRoot}(F_{ck})$	$K2 \times \text{SquareRoot}(F_{ck}) * (Hw/Lw + 1) / (Hw/Lw - 1)$
K1	0.2	-
K2	-	0.045
Tc (N/sqmm)	2.7925	0.838
Tcmin	$K3 \times \text{SquareRoot}(F_{ck})$	
K3	-	0.15
Tcmin (N/sqmm)	-	0.8216
Hence Design Tc (N/sqmm)	-	0.838
Tcmax	0.17 x Fck	

	5.1	5.1
	$T_e < T_{max}$	$T_e < T_{max}$
Thus, T_e (N/sqmm)	2.7925	0.838
	Since, $T_v < T_e$	Since, $T_v < T_e$
Shear Links Design	Shear Links Not Required	Shear Links Not Required

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

Diameter of main horizontal steel	=	8	mm
Thus, Spacing	=	125	mm
Spacing of horizontal reinforcement is minimum of following			
$D / 5$	=	244	mm
$3 \times B$	=	900	mm
Maximum	=	450	mm
Spacing considered	=	125	mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone
Link Dia.	8	---	---	8	---
Spacing	125	---	---	125	---

Secondary Links:

Other link T8@125c/c

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	GRADE BEAM To GFR	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	300	mm
Wall D	=	1220	mm
Clear Cover	=	40	mm

Clear Floor Height @ B	=	2235	mm
Clear Floor Height @ D	=	2235	mm
No Of Floors	=	1	
No Of Walls In Group	=	1	
Wall Type	:	UnBraced	
Minimum eccentricity check	:	One Axis at a Time	
Code defined D/B ratio	:	4	
D/B Ratio	:	4.07 $\geq$ 4 Hence, Design as Wall	

Flexural Design (Analysis Forces)

Analysis Reference No.	=	C1	
Load Combination	=	[29] : 1.5 (DL) -1.5 (EQ-X)	
Critical Location	=	Bottom Joint	
Pu	=	2237.76	kN
Mux	=	992.33	kNm
Muy	=	-49.39	kNm
Vux	=	-55.98	kN
Vuy	=	291.53	kN

Effective Length Calculation

Calculation Along Major Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	1657.635	No Beam	11790 x 230 x 450	-	16.228	0.998
Top	1657.635	No Beam	11790 x 230 x 765	-	79.727	0.973

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Major Axis = 0.99

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	100.233	No Beam	10200 x 230 x 450	-	18.757	0.955
Top	100.233	No Beam	10200 x 230 x 765	-	92.156	0.612

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Minor axis = 0.84

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in X-direction

Minimum Eccentricity Along D:

Minimum Eccentricity = Unsupported Length / 500 + D / 30
 = 45.14 mm
 Minimum Eccentricity > 20 mm
 Mminx = Pu x Minimum Eccentricity
 = 101.01 kNm

Slenderness Check

Max Slenderness Ratio(L/B) = 7.45
 < 60 (Hence Ok)

Column Is Unbraced Along D

Slenderness Check Along D:

Effective Length Factor = 0.99
 Slenderness Ratio = Effective Length / D
 = 1.81, Wall not Slender Along D

Column Is Unbraced Along B

Slenderness Check Along B:

Effective Length Factor = 0.84
 Slenderness Ratio = Effective Length / B
 = 6.26, Wall Not Slender Along B

Calculation of Design Moment

Direction	Manalysis	Mmin (Abs)	Mdesign	Mslndx (Abs)	Mdesign-final
	A	B	C	E	F
Major Axis - Mux	992.33	101.01	992.33	0	992.33
Minor Axis - Muy	-49.39	---	-49.39	0	-49.39

Where

- A = Moments directly from analysis
- B = Moments due to minimum eccentricity
- C = Maximum of analysis moment and min. eccentricity = Max (A,B)
- E = Moment due to slenderness effect
- F = Final design Moment = Max(C- Top Bottom , D- Top Bottom) + E

Final Critical Design Forces

Pu	=	2237.76	kN
Mux	=	992.33	kNm
Muy	=	-49.39	kNm

Resultant Moment (Combined Action)

Moment Capacity Check

Pt Calculated	=	0.56	
Reinforcement Provided	=	14-T25 + 12-T20 + 8-T12	
Load Angle	=	$\tan^{-1}(M_{uy}/M_{ux})$	
	=	2.85	deg
MRes	=	993.56	kNm
MCap	=	1017.43	kNm
Capacity Ratio	=	MRes/ MCap	
	=	0.98 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	7-T12	4-T12	7-T12
Ast provided	791.68	452.39	791.68
Pt as % of entire wall	0.22 %	0.12 %	0.22 %
Pt as % of zone	0.88 %	0.24 %	0.88 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load Combination	[26] : 1.5 (DL) + 1.5 (EQ+X)	[32] : 1.5 (DL) - 1.5 (EQ+Y)
Design shear force, Vu (kN)	291.5331	-152.2779
Design shear stress, Tv (N/sqmm)	$V_u / (B \times 0.8 \times D)$	$V_u / (B \times 0.8 \times D)$
	0.9957	0.5201
Pt (%)	0.278	0.278
Height of Wall, Hw (mm)	2235	2235
Length of Wall, Lw (mm)	1220	300
Hw/Lw	1.832	7.45
	> 1	> 1
Thus Shear Strength, Tc	$K2 \times \text{SquareRoot}(F_{ck}) \times (Hw/Lw + 1) / (Hw/Lw - 1)$	
K1	-	-
K2	0.045	0.045
Tc (N/sqmm)	0.839	0.3229
Tcmin	$K3 \times \text{SquareRoot}(F_{ck})$	
K3	0.15	0.15

T _{min} (N/sqmm)	0.8216	0.8216
Hence Design T _c (N/sqmm)	0.839	0.8216
T _{cmax}	0.17 x F _{ck}	
	5.1	5.1
	T _c < T _{cmax}	T _c < T _{cmax}
Thus, T _c (N/sqmm)	0.839	0.8216
	Since, T _v > T _c	Since, T _v < T _c
Shear Links Design	Shear Links Required	Shear Links Not Required
P _t	0.2781	-
Shear resisted by concrete V _c (kN)	(T _c × e) × (B × D _{eff})	-
	245.66	-
Shear to be resisted by shear reinforcement = V _{us} (kN)	V _u - V _c	
	45.88	-
Area of shear reinforcement required, A _{sv} (sqmm)	(V _{us} × 1000) / (D _{eff} × 0.87 × F _y)	(V _{us} × 1000) / (D _{eff} × 0.87 × F _y)
	600	-
Master Link Rebar (mm)	T8	-
Number of legs provided	2	-
Spacing of links reqd (mm)	167	-
Spacing of links prvd, S _v (mm)	150	-
A _{sv} Provided (sqmm)	670.21	-

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

Diameter of main horizontal steel = 8 mm

Thus, Spacing = 150 mm

Spacing of horizontal reinforcement is minimum of following

D / 5 = 244 mm

3 × B = 900 mm

Maximum = 450 mm

Spacing considered = 150 mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone

Link Dia.	8	8	---	8	---
Spacing	150	168	---	150	---

Secondary Links:

Other link T8@150c/c

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	GFR To FFR	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	230	mm
Wall D	=	1220	mm
Clear Cover	=	40	mm
Clear Floor Height @ B	=	2235	mm
Clear Floor Height @ D	=	2235	mm
No Of Floors	=	1	
No Of Walls In Group	=	1	
Wall Type	:	UnBraced	
Minimum eccentricity check	:	One Axis at a Time	
Code defined D/B ratio	:	4	
D/B Ratio	:	5.3 >= 4 Hence, Design as Wall	

Flexural Design (Analysis Forces)

Analysis Reference No.	=	C1	
Load Combination	=	[29] : 1.5 (DL) -1.5 (EQ-X)	
Critical Location	=	Bottom Joint	
Pu	=	1865.16	kN
Mux	=	834.25	kNm
Muy	=	-91.71	kNm
Vux	=	-62.42	kN
Vuy	=	366.34	kN

Effective Length Calculation

Calculation Along Major Axis Of Column

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Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.973
Top	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Major Axis = 0.98

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	45.168	No Beam	10200 x 230 x 765	-	92.156	0.612
Top	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Minor axis = 0.72

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in X-direction

Minimum Eccentricity Along D:

Minimum Eccentricity = Unsupported Length / 500 + D / 30
= 45.14 mm
Minimum Eccentricity > 20 mm
Mminx = Pu x Minimum Eccentricity
= 84.19 kNm

Slenderness Check

Max Slenderness Ratio(L/B) = 9.72
< 60 (Hence Ok)

Column Is Unbraced Along D

Slenderness Check Along D:

Effective Length Factor = 0.98
Slenderness Ratio = Effective Length / D
= 1.8, Wall not Slender Along D

Column Is Unbraced Along B

Slenderness Check Along B:

Effective Length Factor	=	0.72
Slenderness Ratio	=	Effective Length / B
	=	7, Wall Not Slender Along B

Calculation of Design Moment

Direction	Manalysis	Mmin (Abs)	Mdesign	Mslndx (Abs)	Mdesign-final
	A	B	C	E	F
Major Axis - Mux	834.25	84.19	834.25	0	834.25
Minor Axis - Muy	-91.71	---	-91.71	0	-91.71

Where

- A = Moments directly from analysis
 B = Moments due to minimum eccentricity
 C = Maximum of analysis moment and min. eccentricity = Max (A,B)
 E = Moment due to slenderness effect
 F = Final design Moment = Max(C- Top Bottom , D- Top Bottom) + E

Final Critical Design Forces

Pu	=	1865.16	kN
Mux	=	834.25	kNm
Muy	=	-91.71	kNm

Resultant Moment (Combined Action)**Moment Capacity Check**

Pt Calculated	=	1.02	
Reinforcement Provided	=	14-T25 +12-T20	
Load Angle	=	$\tan^{-1}(Muy/Mux)$	
	=	6.27	deg
MRes	=	839.28	kNm
MCap	=	959.17	kNm
Capacity Ratio	=	MRes/ MCap	
	=	0.88 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	6-T16	4-T12	6-T16
Ast provided	1206.37	452.39	1206.37
Pt as % of entire wall	0.43 %	0.16 %	0.43 %
Pt as % of zone	1.75 %	0.32 %	1.75 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load Combination	[26] : 1.5 (DL) + 1.5 (EQ+X)	[32] : 1.5 (DL) - 1.5 (EQ+Y)
Design shear force, V_u (kN)	366.3371	-159.7374
Design shear stress, T_v (N/sqmm)	$V_u / (B \times 0.8 \times D)$	$V_u / (B \times 0.8 \times D)$
	1.6319	0.7116
Pt (%)	0.511	0.511
Height of Wall, H_w (mm)	2235	2235
Length of Wall, L_w (mm)	1220	230
H_w/L_w	1.832	9.7174
	> 1	> 1
Thus Shear Strength, T_c	$K_2 \times \text{SquareRoot}(F_{ck}) \times (H_w/L_w + 1) / (H_w/L_w - 1)$	
K_1	-	-
K_2	0.045	0.045
T_c (N/sqmm)	0.839	0.303
T_{cmin}	$K_3 \times \text{SquareRoot}(F_{ck})$	
K_3	0.15	0.15
T_{cmin} (N/sqmm)	0.8216	0.8216
Hence Design T_c (N/sqmm)	0.839	0.8216
T_{cmax}	$0.17 \times F_{ck}$	
	5.1	5.1
	$T_c < T_{cmax}$	$T_c < T_{cmax}$
Thus, T_c (N/sqmm)	0.839	0.8216
	Since, $T_v > T_c$	Since, $T_v < T_c$
Shear Links Design	Shear Links Required	Shear Links Not Required
Pt	0.5105	-
Shear resisted by concrete V_c (kN)	$(T_c - e) \times (B \times D_{eff})$	-
	188.34	-
Shear to be resisted by shear reinforcement = V_{us} (kN)	$V_u - V_c$	
	178	-
Area of shear reinforcement required, A_{sv} (sqmm)	$(V_{us} \times 1000) / (D_{eff} \times 0.87 \times F_y)$	$(V_{us} \times 1000) / (B_{eff} \times 0.87 \times F_y)$
	505.13	-
Master Link Rebar (mm)	T8	-
Number of legs provided	2	-
Spacing of links reqd (mm)	199	-

Spacing of links prvd, Sv (mm)	175	-
Asv Provided (sqmm)	574.46	-

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

Diameter of main horizontal steel	=	B	mm
Thus, Spacing	=	175	mm
Spacing of horizontal reinforcement is minimum of following			
D / 5	=	244	mm
3 x B	=	690	mm
Maximum	=	450	mm
Spacing considered	=	175	mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone
Link Dia.	8	8	---	8	---
Spacing	175	199	---	175	---

Secondary Links:

Other link T8@175c/c

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	FFR To SFR	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	230	mm
Wall D	=	1220	mm
Clear Cover	=	40	mm
Clear Floor Height @ B	=	2235	mm
Clear Floor Height @ D	=	2235	mm

No Of Floors = 1
 No Of Walls In Group = 1
 Wall Type : UnBraced
 Minimum eccentricity check : One Axis at a Time
 Code defined D/B ratio : 4
 D/B Ratio : 5.3 >= 4 Hence, Design as Wall

Flexural Design (Analysis Forces)

Analysis Reference No. = C1
 Load Combination = [29] : 1.5 (DL) -1.5 (EQ-X)
 Critical Location = Bottom Joint
 Pu = 1483.93 kN
 Mux = 576.87 kNm
 Muy = -97.34 kNm
 Vux = -64.78 kN
 Vuy = 343.62 kN

Effective Length Calculation

Calculation Along Major Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97
Top	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Major Axis = 0.98

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495
Top	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Minor

$$\text{axis} = 0.69$$

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in X-direction

Minimum Eccentricity Along D:

$$\begin{aligned} \text{Minimum Eccentricity} &= \text{Unsupported Length} / 500 + D / 30 \\ &= 45.14 \quad \text{mm} \\ \text{Minimum Eccentricity} &> 20 \quad \text{mm} \\ M_{\min} &= P_u \times \text{Minimum Eccentricity} \\ &= 66.98 \quad \text{kNm} \end{aligned}$$

Slenderness Check

$$\begin{aligned} \text{Max Slenderness Ratio}(L/B) &= 9.72 \\ &< 60 \quad (\text{Hence Ok}) \end{aligned}$$

Column Is Unbraced Along D

Slenderness Check Along D:

$$\begin{aligned} \text{Effective Length Factor} &= 0.98 \\ \text{Slenderness Ratio} &= \text{Effective Length} / D \\ &= 1.8, \text{ Wall not Slender Along D} \end{aligned}$$

Column Is Unbraced Along B

Slenderness Check Along B:

$$\begin{aligned} \text{Effective Length Factor} &= 0.69 \\ \text{Slenderness Ratio} &= \text{Effective Length} / B \\ &= 6.7, \text{ Wall Not Slender Along B} \end{aligned}$$

Calculation of Design Moment

Direction	Manalysis	Mmin (Abs)	Mdesign	Mslndx (Abs)	Mdesign-final
	A	B	C	E	F
Major Axis - Mux	576.87	66.98	576.87	0	576.87
Minor Axis - Muy	-97.34	---	-97.34	0	-97.34

Where

- A = Moments directly from analysis
- B = Moments due to minimum eccentricity
- C = Maximum of analysis moment and min. eccentricity = Max (A,B)
- E = Moment due to slenderness effect
- F = Final design Moment = Max(C- Top Bottom, D- Top Bottom) + E

Final Critical Design Forces

$$\begin{aligned} P_u &= 1483.93 \quad \text{kN} \\ M_{ux} &= 576.87 \quad \text{kNm} \\ M_{uy} &= -97.34 \quad \text{kNm} \end{aligned}$$

Resultant Moment (Combined Action)**Moment Capacity Check**

Pt Calculated	=	0.64	
Reinforcement Provided	=	14-T25 + 12-T20	
Load Angle	=	$\tan^{-1}(M_{uy}/M_{ux})$	
	=	9.58	deg
MRes	=	585.02	kNm
MCap	=	778.8	kNm
Capacity Ratio	=	MRes/ MCap	
	=	0.75 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	6-T12	4-T12	6-T12
Ast provided	678.58	452.39	678.58
Pt as % of entire wall	0.24 %	0.16 %	0.24 %
Pt as % of zone	0.98 %	0.32 %	0.98 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load Combination	[26] : 1.5 (DL) + 1.5 (EQ+X)	[32] : 1.5 (DL) - 1.5 (EQ+Y)
Design shear force, Vu (kN)	343.6223	-166.838
Design shear stress, Tv (N/sqmm)	$V_u / (B \times 0.8 \times D)$	$V_u / (B \times 0.8 \times D)$
	1.5307	0.7432
Pt (%)	0.322	0.322
Height of Wall, Hw (mm)	2235	2235
Length of Wall, Lw (mm)	1220	230
Hw/Lw	1.832	9.7174
	> 1	> 1
Thus Shear Strength, Tc	$K_2 \times \text{SquareRoot}(F_{ck}) \times (Hw/Lw + 1) / (Hw/Lw - 1)$	
K1	-	-
K2	0.045	0.045
Tc (N/sqmm)	0.839	0.303
Temin	$K_3 \times \text{SquareRoot}(F_{ck})$	
K3	0.15	0.15
Temin (N/sqmm)	0.8216	0.8216
Hence Design Tc (N/sqmm)	0.839	0.8216
Tcmax	0.17 x Fck	

	5.1	5.1
	$T_c < T_{cmax}$	$T_c < T_{cmax}$
Thus, T_c (N/sqmm)	0.839	0.8216
	Since, $T_v > T_c$	Since, $T_v < T_c$
Shear Links Design	Shear Links Required	Shear Links Not Required
P_t	0.3225	-
Shear resisted by concrete V_c (kN)	$(T_c \cdot e) \times (B \times Deff)$	-
	188.34	-
Shear to be resisted by shear reinforcement = V_{us} (kN)	$V_u - V_c$	
	155.29	-
Area of shear reinforcement required, A_{sv} (sqmm)	$(V_{us} \times 1000) / (Deff \times 0.87 \times F_y)$	$(V_{us} \times 1000) / (Beff \times 0.87 \times F_y)$
	460	-
Master Link Rebar (mm)	T8	-
Number of legs provided	2	-
Spacing of links reqd (mm)	218	-
Spacing of links prvd, S_v (mm)	200	-
A_{sv} Provided (sqmm)	502.65	-

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

Diameter of main horizontal steel = 8 mm

Thus, Spacing = 200 mm

Spacing of horizontal reinforcement is minimum of following

$D / 5$ = 244 mm

$3 \times B$ = 690 mm

Maximum = 450 mm

Spacing considered = 200 mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone
Link Dia.	8	8	---	8	---
Spacing	200	219	---	200	---

Secondary Links:

Other link

T8@200c/c

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	SFR To TFR	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	230	mm
Wall D	=	1220	mm
Clear Cover	=	40	mm
Clear Floor Height @ B	=	2235	mm
Clear Floor Height @ D	=	2235	mm
No Of Floors	=	1	
No Of Walls In Group	=	1	
Wall Type	:	UnBraced	
Minimum eccentricity check	:	One Axis at a Time	
Code defined D/B ratio	:	4	
D/B Ratio	:	5.3 >= 4 Hence, Design as Wall	

Flexural Design (Analysis Forces)

Analysis Reference No.	=	C1	
Load Combination	=	[31] : 1.5 (DL) +1.5 (EQ-Y)	
Critical Location	=	Bottom joint	
Pu	=	1097.37	kN
Mux	=	272.18	kNm
Muy	=	-230.5	kNm
Vux	=	-155.28	kN
Vuy	=	196.25	kN

Effective Length Calculation

Calculation Along Major Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	

Bottom	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97
Top	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Major Axis = 0.98

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495
Top	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Minor axis = 0.69

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in X-direction

Minimum Eccentricity Along D:

Minimum Eccentricity = Unsupported Length / 500 + D / 30
= 45.14 mm
Minimum Eccentricity > 20 mm
Mminx = Pu x Minimum Eccentricity
= 49.53 kNm

Slenderness Check

Max Slenderness Ratio(L/B) = 9.72
< 60 (Hence Ok)

Column Is Unbraced Along D

Slenderness Check Along D:

Effective Length Factor = 0.98
Slenderness Ratio = Effective Length / D
= 1.8, Wall not Slender Along D

Column Is Unbraced Along B

Slenderness Check Along B:

Effective Length Factor = 0.69
Slenderness Ratio = Effective Length / B
= 6.7, Wall Not Slender Along B

Calculation of Design Moment

Direction	Manalysis	Mmin (Abs)	Mdesign	Mslindx (Abs)	Mdesign-final
	A	B	C	E	F
Major Axis - Mux	272.18	49.53	272.18	0	272.18
Minor Axis - Muy	-230.5	---	-230.5	0	-230.5

Where

- A = Moments directly from analysis
B = Moments due to minimum eccentricity
C = Maximum of analysis moment and min. eccentricity = Max (A,B)
E = Moment due to slenderness effect
F = Final design Moment = Max(C- Top Bottom , D- Top Bottom) + E

Final Critical Design Forces

Pu	=	1097.37	kN
Mux	=	272.18	kNm
Muy	=	-230.5	kNm

Resultant Moment (Combined Action)

Moment Capacity Check

Pt Calculated	=	0.64	
Reinforcement Provided	=	14-T25 +12-T20	
Load Angle	=	$\tan^{-1}(Muy/Mux)$	
	=	40.26	deg
MRes	=	356.67	kNm
MCap	=	569.02	kNm
Capacity Ratio	=	MRes/ MCap	
	=	0.63 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	6-T12	4-T12	6-T12
As _t provided	678.58	452.39	678.58
Pt as % of entire wall	0.24 %	0.16 %	0.24 %
Pt as % of zone	0.98 %	0.32 %	0.98 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load	[26] : 1.5 (DL) +1.5	[32] : 1.5 (DL) -1.5

Combination	(EQ+X)	(EQ+Y)
Design shear force, V_u (kN)	322.4764	-155.2845
Design shear stress, T_v (N/sqmm)	$V_u / (B \times 0.8 \times D)$	$V_u / (B \times 0.8 \times D)$
	1.4365	0.6918
Pt (%)	0.322	0.322
Height of Wall, H_w (mm)	2235	2235
Length of Wall, L_w (mm)	1220	230
H_w/L_w	1.832	9.7174
	> 1	> 1
Thus Shear Strength, T_c	$K_2 \times \text{SquareRoot}(F_{ck}) \times (H_w/L_w + 1) / (H_w/L_w - 1)$	
K_1	-	-
K_2	0.045	0.045
T_c (N/sqmm)	0.839	0.303
T_{min}	$K_3 \times \text{SquareRoot}(F_{ck})$	
K_3	0.15	0.15
T_{min} (N/sqmm)	0.8216	0.8216
Hence Design T_c (N/sqmm)	0.839	0.8216
T_{max}	$0.17 \times F_{ck}$	
	5.1	5.1
	$T_c < T_{max}$	$T_c < T_{max}$
Thus, T_c (N/sqmm)	0.839	0.8216
	Since, $T_v > T_c$	Since, $T_v < T_c$
Shear Links Design	Shear Links Required	Shear Links Not Required
Pt	0.3225	-
Shear resisted by concrete V_c (kN)	$(T_c - e) \times (B \times D_{eff})$	-
	188.34	-
Shear to be resisted by shear reinforcement = V_{us} (kN)	$V_u - V_c$	
	134.14	-
Area of shear reinforcement required, A_{sv} (sqmm)	$(V_{us} \times 1000) / (D_{eff} \times 0.87 \times F_y)$	$(V_{us} \times 1000) / (B_{eff} \times 0.87 \times F_y)$
	460	-
Master Link Rebar (mm)	T8	-
Number of legs provided	2	-
Spacing of links reqd (mm)	218	-
Spacing of links prvd, S_v (mm)	200	-
A_{sv} Provided (sqmm)	502.65	-

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

Diameter of main horizontal steel	=	8	mm
Thus, Spacing	=	200	mm
Spacing of horizontal reinforcement is minimum of following			
D / 5	=	244	mm
3 x B	=	690	mm
Maximum	=	450	mm
Spacing considered	=	200	mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone
Link Dia.	8	8	---	8	---
Spacing	200	219	---	200	---

Secondary Links:

Other link T8@200c/c

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	TFR To 4FR	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	230	mm
Wall D	=	1220	mm
Clear Cover	=	40	mm
Clear Floor Height @ B	=	2235	mm
Clear Floor Height @ D	=	2235	mm
No Of Floors	=	1	
No Of Walls In Group	=	1	
Wall Type	:	UnBraced	
Minimum eccentricity check	:	One Axis at a Time	
Code defined D/B ratio	:	4	

D/B Ratio : 5.3 $\geq$ 4 Hence, Design as Wall

Flexural Design (Analysis Forces)

Analysis Reference No. = C1
 Load Combination = [31] : 1.5 (DL) + 1.5 (EQ-Y)
 Critical Location = Bottom Joint
 Pu = 710.22 kN
 Mux = 224.74 kNm
 Muy = -198.35 kNm
 Vux = -133.23 kN
 Vuy = 165.09 kN

Effective Length Calculation

Calculation Along Major Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97
Top	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Major Axis = 0.98

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495
Top	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495

Sway Condition (as per Stability Index) = Non Sway

Effective Length Factor along Minor axis = 0.69

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in X-direction

Minimum Eccentricity Along D:

$$\begin{aligned} \text{Minimum Eccentricity} &= \text{Unsupported Length} / 500 + D / 30 \\ &= 45.14 \quad \text{mm} \\ \text{Minimum Eccentricity} &> 20 \quad \text{mm} \\ M_{\min} &= P_u \times \text{Minimum Eccentricity} \\ &= 32.06 \quad \text{kNm} \end{aligned}$$

Slenderness Check

$$\begin{aligned} \text{Max Slenderness Ratio}(L/B) &= 9.72 \\ &< 60 \quad (\text{Hence Ok}) \end{aligned}$$

Column Is Unbraced Along D

Slenderness Check Along D:

$$\begin{aligned} \text{Effective Length Factor} &= 0.98 \\ \text{Slenderness Ratio} &= \text{Effective Length} / D \\ &= 1.8, \text{ Wall not Slender Along D} \end{aligned}$$

Column Is Unbraced Along B

Slenderness Check Along B:

$$\begin{aligned} \text{Effective Length Factor} &= 0.69 \\ \text{Slenderness Ratio} &= \text{Effective Length} / B \\ &= 6.7, \text{ Wall Not Slender Along B} \end{aligned}$$

Calculation of Design Moment

Direction	Manalysis	Mmin (Abs)	Mdesign	Mslndx (Abs)	Mdesign-final
	A	B	C	E	F
Major Axis - Mux	224.74	32.06	224.74	0	224.74
Minor Axis - Muy	-198.35	---	-198.35	0	-198.35

Where

- A = Moments directly from analysis
- B = Moments due to minimum eccentricity
- C = Maximum of analysis moment and min. eccentricity = Max (A,B)
- E = Moment due to slenderness effect
- F = Final design Moment = Max(C- Top Bottom , D- Top Bottom) + E

Final Critical Design Forces

$$\begin{aligned} P_u &= 710.22 \quad \text{kN} \\ M_{ux} &= 224.74 \quad \text{kNm} \\ M_{uy} &= -198.35 \quad \text{kNm} \end{aligned}$$

Resultant Moment (Combined Action)

Moment Capacity Check

$$P_t \text{ Calculated} = 0.64$$

Reinforcement Provided	=	14-T25 + 12-T20	
Load Angle	=	$\tan^{-1}(M_{uy}/M_{ux})$	
	=	41.43	deg
MRes	=	299.75	kNm
MCap	=	506.51	kNm
Capacity Ratio	=	MRes/ MCap	
	=	0.59 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	6-T12	4-T12	6-T12
Ast provided	678.58	452.39	678.58
Pt as % of entire wall	0.24 %	0.16 %	0.24 %
Pt as % of zone	0.98 %	0.32 %	0.98 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load Combination	[26] : 1.5 (DL) + 1.5 (EQ+X)	[32] : 1.5 (DL) - 1.5 (EQ+Y)
Design shear force, Vu (kN)	260.42	-133.2321
Design shear stress, Tv (N/sqmm)	$V_u / (B \times 0.8 \times D)$	$V_u / (B \times 0.8 \times D)$
	1.1601	0.5935
Pt (%)	0.322	0.322
Height of Wall, Hw (mm)	2235	2235
Length of Wall, Lw (mm)	1220	230
Hw/Lw	1.832	9.7174
	> 1	> 1
Thus Shear Strength, Tc	$K2 \times \text{SquareRoot}(F_{ck}) \times (Hw/Lw + 1) / (Hw/Lw - 1)$	
K1	-	-
K2	0.045	0.045
Tc (N/sqmm)	0.839	0.303
Temin	$K3 \times \text{SquareRoot}(F_{ck})$	
K3	0.15	0.15
Temin (N/sqmm)	0.8216	0.8216
Hence Design Tc (N/sqmm)	0.839	0.8216
Temax	0.17 x Fck	
	5.1	5.1
	Tc < Temax	Tc < Temax
Thus, Tc (N/sqmm)	0.839	0.8216
	Since, Tv > Tc	Since, Tv < Tc
Shear Links Design	Shear Links Required	Shear Links Not

		Required
Pt	0.3225	-
Shear resisted by concrete V_c (kN)	$(T_c - e) \times (B \times D_{eff})$	-
	188.34	-
Shear to be resisted by shear reinforcement = V_{us} (kN)	$V_u - V_c$	
	72.08	-
Area of shear reinforcement required, A_{sv} (sqmm)	$(V_{us} \times 1000) / (D_{eff} \times 0.87 \times F_y)$	$(V_{us} \times 1000) / (B_{eff} \times 0.87 \times F_y)$
	460	-
Master Link Rebar (mm)	T8	-
Number of legs provided	2	-
Spacing of links reqd (mm)	218	-
Spacing of links prvd, S_v (mm)	200	-
A_{sv} Provided (sqmm)	502.65	-

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

Diameter of main horizontal steel	=	8	mm
Thus, Spacing	=	200	mm
Spacing of horizontal reinforcement is minimum of following			
$D / 5$	=	244	mm
$3 \times B$	=	690	mm
Maximum	=	450	mm
Spacing considered	=	200	mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone
Link Dia.	8	8	---	8	---
Spacing	200	219	---	200	---

Secondary Links:

Other link T8@200c/c

General Data

Wall No.	:	C1	
Frame Type	=	Non-Ductile	
Level	:	4FR To 5FR	
Design Code	=	IS 456 - 2000 + IS 13920 - 2016	
Grade Of Concrete	=	M30	N/sqmm
Grade Of Steel (Main)	=	Fe550	N/sqmm
Grade Of Steel (Shear)	=	Fe415	N/sqmm
Grade Of Steel - Flexural Design	=	Fe550	N/sqmm
Grade Of Steel - Shear Design	=	Fe415	N/sqmm
Wall B	=	230	mm
Wall D	=	1220	mm
Clear Cover	=	40	mm
Clear Floor Height @ B	=	2235	mm
Clear Floor Height @ D	=	2235	mm
No Of Floors	=	1	
No Of Walls In Group	=	1	
Wall Type	:	UnBraced	
Minimum eccentricity check	:	One Axis at a Time	
Code defined D/B ratio	:	4	
D/B Ratio	:	5.3 $\geq$ 4 Hence, Design as Wall	

Flexural Design (Analysis Forces)

Analysis Reference No.	=	C1	
Load Combination	=	[29] : 1.5 (DL) - 1.5 (EQ-X)	
Critical Location	=	Top Joint	
Pu	=	326.79	kN
Mux	=	-450.77	kNm
Muy	=	65.5	kNm
Vux	=	-77.2	kN
Vuy	=	320.87	kN

Effective Length Calculation**Calculation Along Major Axis Of Column**

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.97
Top	1270.853	No Beam	11790 x 230 x 765	-	79.727	0.941

Sway Condition (as per Stability)

Index) = Non Sway
 Effective Length Factor along Major Axis = 0.96

Calculation Along Minor Axis Of Column

Joint	Column Stiffness	Beam Sizes		Beam Stiffness		Beta
		Beam 1 (Length x Width x Depth)	Beam 2 (Length x Width x Depth)	Beam 1	Beam 2	
	N-m x 10 ⁶	mm	mm	N-m x 10 ⁶	N-m x 10 ⁶	
Bottom	45.168	No Beam	10200 x 230 x 765	-	92.156	0.495
Top	45.168	No Beam	10200 x 230 x 765	-	92.156	0.329

Sway Condition (as per Stability Index) = Non Sway
 Effective Length Factor along Minor axis = 0.64

Minimum Eccentricity Check

Since Axial Force is compressive, Min. Eccentricity check to be performed

Most critical case is with Min. Eccentricity check in X-direction

Minimum Eccentricity Along D:

Minimum Eccentricity = Unsupported Length / 500 + D / 30
 = 45.14 mm
 Minimum Eccentricity > 20 mm
 Mminx = Pu x Minimum Eccentricity
 = 14.75 kNm

Slenderness Check

Max Slenderness Ratio(L/B) = 9.72
 < 60 (Hence Ok)

Column Is Unbraced Along D

Slenderness Check Along D:

Effective Length Factor = 0.96
 Slenderness Ratio = Effective Length / D
 = 1.76, Wall not Slender Along D

Column Is Unbraced Along B

Slenderness Check Along B:

Effective Length Factor = 0.64
 Slenderness Ratio = Effective Length / B
 = 6.22, Wall Not Slender Along B

Calculation of Design Moment

Direction	Manalysis	Mmin (Abs)	Mdesign	Mslndx (Abs)	Mdesign-final
	A	B	C	E	F

Major Axis - Mux	-450.77	14.75	-450.77	0	-450.77
Minor Axis - Muy	65.5	---	65.5	0	65.5

Where

- A = Moments directly from analysis
 B = Moments due to minimum eccentricity
 C = Maximum of analysis moment and min. eccentricity = $\text{Max} (A, B)$
 E = Moment due to slenderness effect
 F = Final design Moment = $\text{Max}(C\text{- Top Bottom}, D\text{- Top Bottom}) + E$

Final Critical Design Forces

Pu	=	326.79	kN
Mux	=	-450.77	kNm
Muy	=	65.5	kNm

Resultant Moment (Combined Action)

Moment Capacity Check

Pt Calculated	=	0.64	
Reinforcement Provided	=	14-T25 + 12-T20	
Load Angle	=	$\text{Tan}^{-1}(\text{Muy/Mux})$	
	=	8.27	deg
MRes	=	455.51	kNm
MCap	=	562.2	kNm
Capacity Ratio	=	$\text{MRes} / \text{MCap}$	
	=	0.81 <= 1	

Wall Configuration

	Z1	Mid	Z1
Length (mm)	300	620	300
Reinforcement	6-T12	4-T12	6-T12
Ast provided	678.58	452.39	678.58
Pt as % of entire wall	0.24 %	0.16 %	0.24 %
Pt as % of zone	0.98 %	0.32 %	0.98 %

Design Of Shear

Shear Calculation	Along D	Along B
Critical Load Combination	[1] : 1.5 (DL) + 1.5 (LL)	[32] : 1.5 (DL) - 1.5 (EQ + Y)
Design shear force, Vu (kN)	330.6075	-130.2947
Design shear stress, Tv (N/sqmm)	$\text{Vu} / (\text{B} \times 0.8 \times \text{D})$	$\text{Vu} / (\text{B} \times 0.8 \times \text{D})$

	1.4728	0.5804
Pt (%)	0.322	0.322
Height of Wall, Hw (mm)	2235	2235
Length of Wall, Lw (mm)	1220	230
Hw/Lw	1.832	9.7174
	> 1	> 1
Thus Shear Strength, Tc	$K2 \times \text{SquareRoot}(F_{ck}) \times (Hw/Lw + 1) / (Hw/Lw - 1)$	
K1	-	-
K2	0.045	0.045
Tc (N/sqmm)	0.839	0.303
Tcmin	$K3 \times \text{SquareRoot}(F_{ck})$	
K3	0.15	0.15
Tcmin (N/sqmm)	0.8216	0.8216
Hence Design Tc (N/sqmm)	0.839	0.8216
Tcmax	0.17 x Fck	
	5.1	5.1
	Tc < Tcmax	Tc < Tcmax
Thus, Tc (N/sqmm)	0.839	0.8216
	Since, Tv > Tc	Since, Tv < Tc
Shear Links Design	Shear Links Required	Shear Links Not Required
Pt	0.3225	-
Shear resisted by concrete Vc (kN)	$(Tc \times e) \times (B \times Deff)$	-
	188.34	-
Shear to be resisted by shear reinforcement = Vus (kN)	$V_u - V_c$	
	142.27	-
Area of shear reinforcement required, Asv (sqmm)	$(V_{us} \times 1000) / (Deff \times 0.87 \times F_y)$	$(V_{us} \times 1000) / (Beff \times 0.87 \times F_y)$
	460	-
Master Link Rebar (mm)	T8	-
Number of legs provided	2	-
Spacing of links reqd (mm)	218	-
Spacing of links prvd, Sv (mm)	200	-
Asv Provided (sqmm)	502.65	-

Design Of Links

Main Links

Links in the zone where special confining links are not required

Normal Links

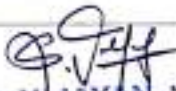
Diameter of main horizontal steel	=	8	mm
Thus, Spacing	=	200	mm
Spacing of horizontal reinforcement is minimum of following			
D / 5	=	244	mm
3 x B	=	690	mm
Maximum	=	450	mm
Spacing considered	=	200	mm

Table For Links

	Required			Provided	
	Normal Design	Shear Design	Ductile Design	Normal Zone	Ductile Zone
Link Dia.	8	8	---	8	---
Spacing	200	219	---	200	---

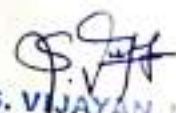
Secondary Links:

Other link T8@200c/c


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GRADE BEAM DESIGN CALCULATION

Sr.No.	Symbol	Definitions
1	α	= Angle formed with horizontal by diagonal reinforcement
2	ϵ_l	= Strain at level considered, Calculated ignoring the stiffening of the concrete in tension zone
3	ϵ_m	= Average steel strain at level considered
4	A_{cr}	= Distance from the point considered to the surface of the nearest longitudinal bar
5	A_{dr}	= Area of diagonal reinforcement in coupler beam
6	A_{stCalc}	= Area of Tension reinforcement required in sqmm
7	$A_{st comp}$	= A_{st} at compression side
8	$A_{stCrack}$	= Area of Tension reinforcement for Crack Width required in sqmm
9	A_{stPrv}	= Area of reinforcement provided at given section in sqmm
10	A_{sv}	= Area of shear reinforcement required per meter length in sqmm
11	$A_{sv Reqd}$	= Min area shear reinforcement as per clause 41.4.3
12	$A_{sv Total Prv}$	= Total area of shear reinforcement provided, including that for torsion
13	$A_{sv Torsion}$	= Area of Stirrups over the corner bars to resist shear and torsion as per clause 41.4.3
14	$A_{sv Torsion Prv}$	= Area of shear reinforcement resisting torsion (outer legs only)
15	b	= Width of the Beam in mm
16	b_w	= Width of Web in mm
17	C_{eff}	= Effective Cover of Beam in mm
18	C_{min}	= Clear cover to top and bottom reinforcement in mm
19	C_{side}	= Clear cover to side reinforcement in mm
20	d	= Effective depth of Beam in mm
21	d'	= Clear cover to reinforcement at compression side.
22	D	= Depth of Beam in mm
23	D'	= Distance (c/c) between top-most and bottom-most layer
24	D_f	= Thickness of Flange in mm
25	E_c	= Modulus of elasticity of concrete
26	E_s	= Modulus of elasticity of steel


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27	FcPerm	=	Permissible Stress in Concrete required in N/sqmm
28	Fst	=	Stress in steel
29	FstPerm	=	Permissible Stress in Steel required in N/sqmm
30	Legs	=	Number of legs of the shear reinforcement
31	lo	=	Effective Length of Beam in mm
32	Mh	=	Hogging Moment of Resistance in kNm
33	Ms	=	Sagging Moment of Resistance in kNm
34	M _{Tu}	=	Converted Bending Moment due to Torsion at a section in kNm
35	Mu	=	Factored Bending Moment in Limit State at a section in kNm
36	Mud	=	Total Design Moment = Mu + M _{Tu} in kNm
37	MuLim	=	Limiting Moment of Resistance of Singly Reinforced Section
38	NA angle (φ)	=	It is a neutral axis angle corresponding to load angle to find out MCap
39	Pcclc	=	Calculated percentage compression steel
40	Ptcclc	=	Calculated percentage tension steel
41	Ptmin	=	Minimum percentage steel as per code
42	PtPrv	=	provided percentage steel
43	R	=	Moment Ratio Mud/Bd ²
44	Reinf	=	Rebar arrangement provided
45	sp	=	Spacing Between bars at outer most layer
46	Spc1 to Spc6	=	Max Stirrup Criteria in mm
47	Stirrup Dia	=	Diameter of shear stirrups in mm
48	SvCalc	=	Stirrup spacing calculated as per Asv in mm
49	SvPrv	=	Stirrup spacing provided in m
50	Tc	=	Permissible Shear stress in concrete at a given section in N/sqmm Calculated as per Tensile reinforcement
51	Tce	=	Earthquake induced shear stress in N/sqmm
52	Tren	=	Permissible value of shear stress for checking of coupling action in N/sqmm
53	Tu	=	Factored Torsional Moment in Limit State at a section in kNm
54	Tv	=	Shear stress due to Vud in N/sqmm
55	V ^{D+L}	=	Shear force 1.2x(Dead Load + Live Load) in kN
56	Vc	=	Shear capacity of concrete section due to Tc in kN
57	Vu	=	Factored Shear Force in Limit State at a section in kN
58	Vu-A1	=	V ^{D+L} Left - 1.4 x (MsLeft + MhRight)/L in kN
59	Vu-A2	=	V ^{D+L} Left + 1.4 x (MhLeft + MsRight)/L in kN
60	Vu-B1	=	V ^{D+L} Right + 1.4 x (MsLeft + MhRight)/L in kN
61	Vu-B2	=	V ^{D+L} Right - 1.4 x (MhLeft + MsRight)/L in kN
62	Vud	=	Design Shear Force (Max of Vus and Vu-sway) in kN
63	Vue	=	Earthquake induced shear in kN
64	Vu-sway	=	Max of (Vu-A1 and Vu-A2) & (Vu-B1 and Vu-B2) in kN
65	Vus	=	Vud - Vc Design Shear Force for reinforcement, in kN

66	V_{ut}	=	Total Shear Force = $V_u + V_{Tu}$ in kN
67	V_{Tu}	=	Converted Shear Force due to Torsion at a section in kN
68	W_{cr}	=	Surface Crack Width
69	W_{crPerm}	=	Permissible Crack Width required in mm
70	X_1	=	Smaller c/c dimension of outermost Stirrups
71	Y_1	=	Larger c/c dimension of outermost Stirrups

All 6mm diameter bars are assumed 250 grade with $f_y = 250$ N/sqmm

All Forces are in 'kN', 'kNm', Stress in 'N/sqmm' & Dimension are in 'mm'.

Code References

IS 456

Sr.No.	Item	Clause / Table
1.	P_{tmax}	: 26.5.1.1
2.	P_{tmin}	: 26.5.1.1
3.	M_{Tu}	: 41.4.2
4.	V_{Tu}	: 41.3.1
5.	P_{tcl}	: 38
6.	T_c	: 40.2.1
7.	T_{cmax}	: 40.2.3
8.	A_{sv}	: 40.4
9.	Min Shear Reinf	: 26.5.1.6
10.	Max Stirrup Spacing	: 26.5.1.5
11.	Shear Reinf - Torsion	: 26.5.1.7
12.	Side Face Reinforcement	: 26.5.1.3
13.	crack width calculation	: Annex-F
14.	cracking	: Clause 35.3.2

IS 13920 - 2016

Sr.No.	Item	Clause / Table
1.	P_{tmax}	: 6.2.2
2.	P_{tmin}	: 6.2.1
3.	A_{stmin}	: 6.2.3 & 6.2.4
4.	S_{vcl}	: 6.3.5
5.	Shear Capacity	: 6.3.4
6.	Coupling Beams	: 10.5

Group : G6
 Beam No : G B 2 A
 Analysis Reference (Member) : 69,81 (0 m)
 Beam Length : 580 mm
 Breadth (B) : 300 mm
 Depth (D) : 450 mm
 Effective Depth (d) : 395 mm
 Design Code : IS 456 : 2000 + IS 13920 : 2016
 Beam Type : Ductile Beam
 Grade Of Concrete (Fck) : M30 N/sqmm
 Grade Of Steel (Main) : Fe550 N/sqmm
 Grade Of Steel (Shear) : Fe415 N/sqmm
 Top/Bottom Clear Cover (Cmin) : 25 mm
 Side Clear Cover : 25 mm
 Es : 2×10^5 N/sqmm
 Ptnominal (%) (Bn) : 0.21 %

Flexure Design						
	Beam Bottom			Beam Top		
	Left	Mid	Right	Left	Mid	Right
Critical L/C - Analysis	406	406	407	407	406	406
Critical L/C - RCDC	31	31	32	32	31	31
Mu (kNm)	10.58	11.06	9.14	34.19	11.9	35.87
Tu (kNm)	0.31	0.31	0.23	1.19	0.31	0.31
M _{Tu} (kNm)	0.54	0.54	0.4	2.08	0.54	0.54
Mud (kNm)	11.12	11.61	9.54	36.27	12.44	36.41
MuLim (kNm)	117	117	117	117	117	117
R	0.31	0.323	0.266	1.011	0.347	1.015
Ptmin (%) (A)	0.218	0.218	0.218	0.218	0.218	0.218
Ptcll (%) (B')	0.218	0.218	0.218	0.222	0.218	0.223
Pcccl (%) (C)	0	0	0	0	0	0
PtPrv (%)	0.373	0.373	0.373	0.373	0.373	0.373
Ast (sqmm)	198.22	198.22	198.22	201.8	198.22	202.63
AstDuctile (sqmm) (E)	169.65	84.82	169.65	84.82	84.82	84.82
AstFinal (Max(Ast, AstDuctile)) (sqmm)	198.22	198.22	198.22	201.8	198.22	202.63
AstPrv (sqmm)	339.3	339.3	339.3	339.3	339.3	339.3
Reinforcement Provided	3-T16	3-T16	3-T16	3-T16	3-T16	3-T16

Note: Calculation of Ast

AstCalc

$$= \text{Max } \{B', C\} \times B \times d \text{ (for } \mu > 0 \text{)}$$

AstCalc

$$= B_n \times B \times d \text{ (for } \mu = 0 \text{)}$$

Where,

A

$$= P_{tmin}$$

= Min % area of flexural reinforcement
Maximum of % reinforcement required for Bending

B'

$$= P_{tcl}$$

= Moment and Min % area of flexural reinforcement (A)

B_n

$$= P_{tnominal}$$

= Nominal % area of reinforcement

C

$$= P_{ccl}$$

= % area of compression reinforcement required

D

$$= A_{stCrack}$$

= Area of reinforcement required for Crackwidth

E

$$= A_{stDuctile}$$

= Area of reinforcement as per ductile detailing requirements

Ductile Detailing

AstDuctile - Bottom (left & Right)

= Max(50% of Ast provided at top, 25% of max Ast provided from all zones)

AstDuctile - Top (left & Right), Bottom (Mid) & Top (Mid)

= 25% of max Ast provided from all zones

Shear Design			
	Left	Mid	Right
Critical L/C - Analysis	409	409	406
Critical L/C - RCDC	34	34	31

PtPrv (%)	0.373	0.373	0.373
Vu (kN)	27.16	23.34	19.09
Tu (kNm)	6.61	6.61	0.31
V _{Tu} (kN)	46	46	2.18
Vut (kN)	73.16	69.34	21.27
V _{prv} (kN)	14.18	11.08	11.53
Mh (kNm)	58.83		58.83
Ms (kNm)	58.83		58.83
Sway-Right (kN)	10.63	13.73	36.34
Sway-Left (kN)	38.99	35.89	14.81
Vu-Sway (kN)	38.99	35.89	36.34
Vud (kN)	73.16	69.34	36.34
Tv (N/sqmm)	0.43	0.76	0.4
Tc (N/sqmm)	0	0	0
Vc (kN)	0	0	0
Vus=Vud-Vc (kN)	73.16	69.34	36.34
Legs	2	2	2
Stirrup Rebar	8	8	8
Asv Torsion (sqmm)	358.506	347.604	67.803
Asv Torsion Prv (sqmm)	1436.29	670.27	1436.29
Asv Reqd (sqmm/m)	512.96	486.19	254.83
SvCalc (mm)	70	150	70
SvPrv (mm)	70	150	70
Asv Total Prv (sqmm)	1436.29	670.27	1436.29

Maximum Spacing Criteria

Basic

Spc1 = 0.75d	=	296	mm
Spc2	=	300	mm

For Torsion

(X1 = 190, Y1 = 410)

Spc3 = X1	=	190	mm
Spc4 = (X1+Y1)/4	=	150	mm

For Ductility

Left Section

Spc5 = d / 4	=	99	mm
Spc6 = 6 x Small Longitudinal Dia	=	70	mm
Spc7	=	100	mm

Mid Section

Spc5 = d / 2	=	198	mm
--------------	---	-----	----

Right Section

Spc5 = $d / 4$ = 99 mm

Spc6 = 6 x Small Longitudinal Dia = 70 mm

Spc7 = 100 mm

SFR Design

Beam Width = 230 mm

Beam Depth = 450 mm

Web Depth = 450 <= 750 mm

Side Face Reinforcement not required.



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CMDA : SE/GR1/2022/11/346

Corporation of Chennai Registered Structural Engineer

GRADE-1 RGN No: RSE101902023

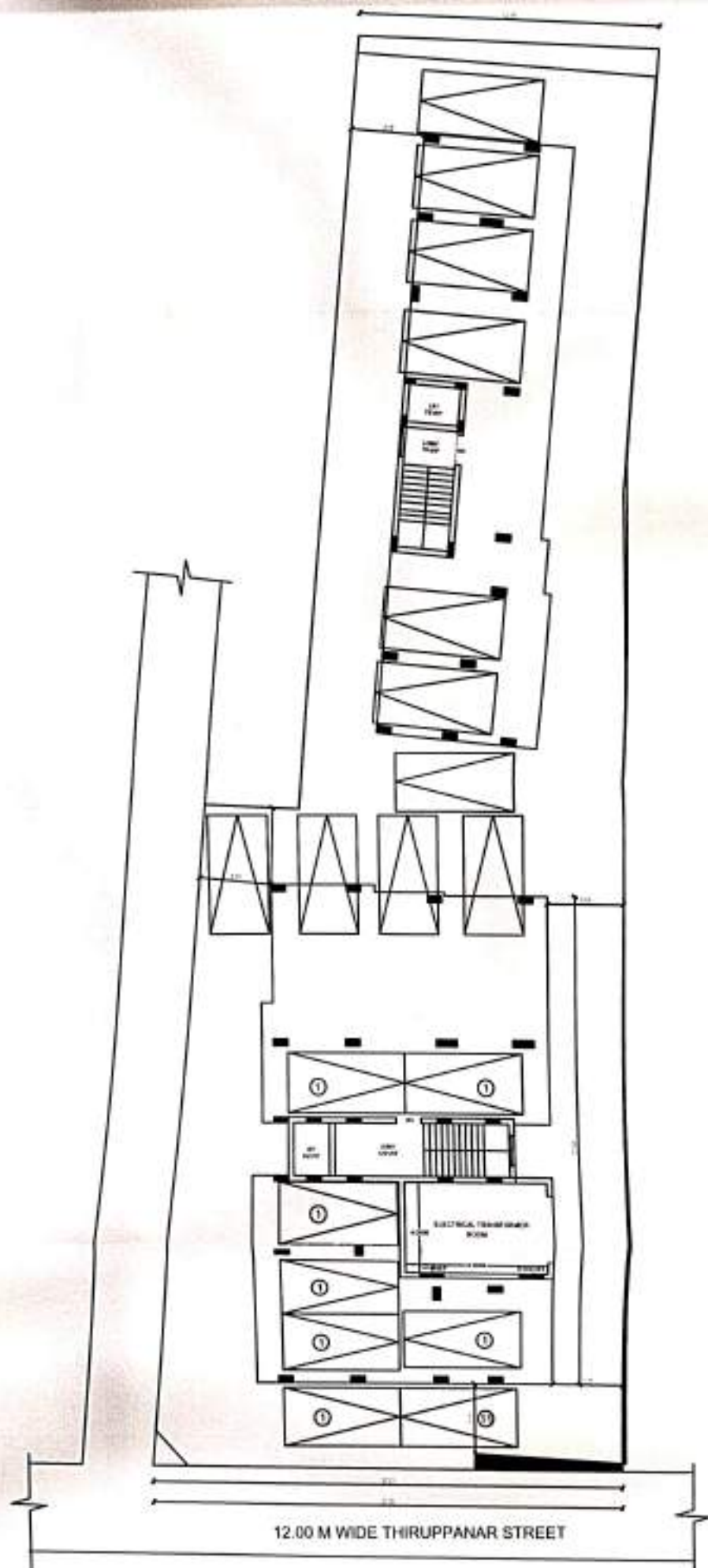
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Email: grandasmithprivatelimited@gmail.com

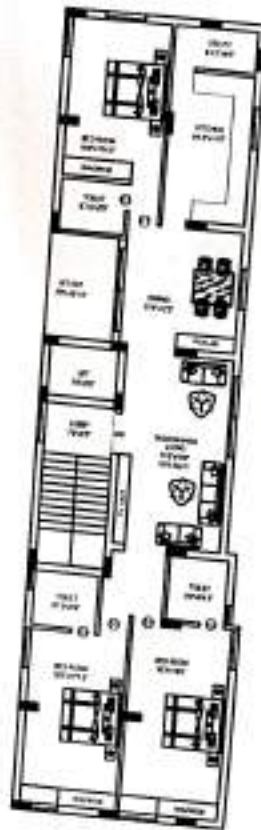
Email: lardseengineering01@gmail.com

FLOORS RESIDENTIAL BUILDING AT MOGAPPAIR



STILT FLOOR

FLOORS RESIDENTIAL BUILDING AT MOGAPPAIR



TYPICAL FLOOR PLAN
FIRST, SECOND, THIRD,
FOURTH AND FIFTH FLOOR



CHENNAI METROPOLITAN DEVELOPMENT AUTHORITY
"Thalamuthu Natarajan Building", No.1, Gandhi Irwin Road,
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PROFESSIONAL REGISTRATION CERTIFICATE

This is to certify that **Thiru. VIJAYAN. S** has enrolled as **Registered Structural Engineer Grade-I (SE)** with Chennai Metropolitan Development Authority (CMDA) who has the qualification of **M.E., (Structural Engg.)** and experience in the relevant field for **5 years**.

He has been given the Registration No.**SE/GR-I/2022/11/346** on **08.11.2022**. He shall be required to comply with the duties and responsibilities prescribed by the Government of Tamil Nadu in Part-V, "Registration of Professionals", Tamil Nadu Combined Development and Building Rules, 2019 approved vide G.O.(Ms) No.18 MAWS (MA1) Dept. dated 04.02.2019.

This Registration is valid upto **07.11.2027**.



(Signature)
(A. MEGANATHAN)
Superintendent



GREATER CHENNAI CORPORATION
TOWN PLANNING DEPARTMENT

PROFESSIONAL REGISTRATION CERTIFICATE

This is to certify that Mr. Vijayan S has been enrolled as Registered Structural Engineer Grade- I (RSE) in Greater Chennai Corporation (GCC) who has the qualification of M.E.(Structural Engg.) with minimum of 5 years experience in the relevant field.

The Registration No. is RSE101902023 dated 08.01.2024. It is informed herewith to comply with the scope of work, duties and responsibilities as prescribed by the Government of Tamil Nadu in Part - V, "Registration of Professionals", Tamil Nadu Combined Development and Building Rules, 2019 approved vide G.O.(Ms) No.18 MA&WS (MA1) Dept. dated 04.02.2019. and as amended in G.O.(MS) No.16 MA&WS (MA1) Dept. dated 31.01.2020.

This Registration is valid upto . 07.01.2029

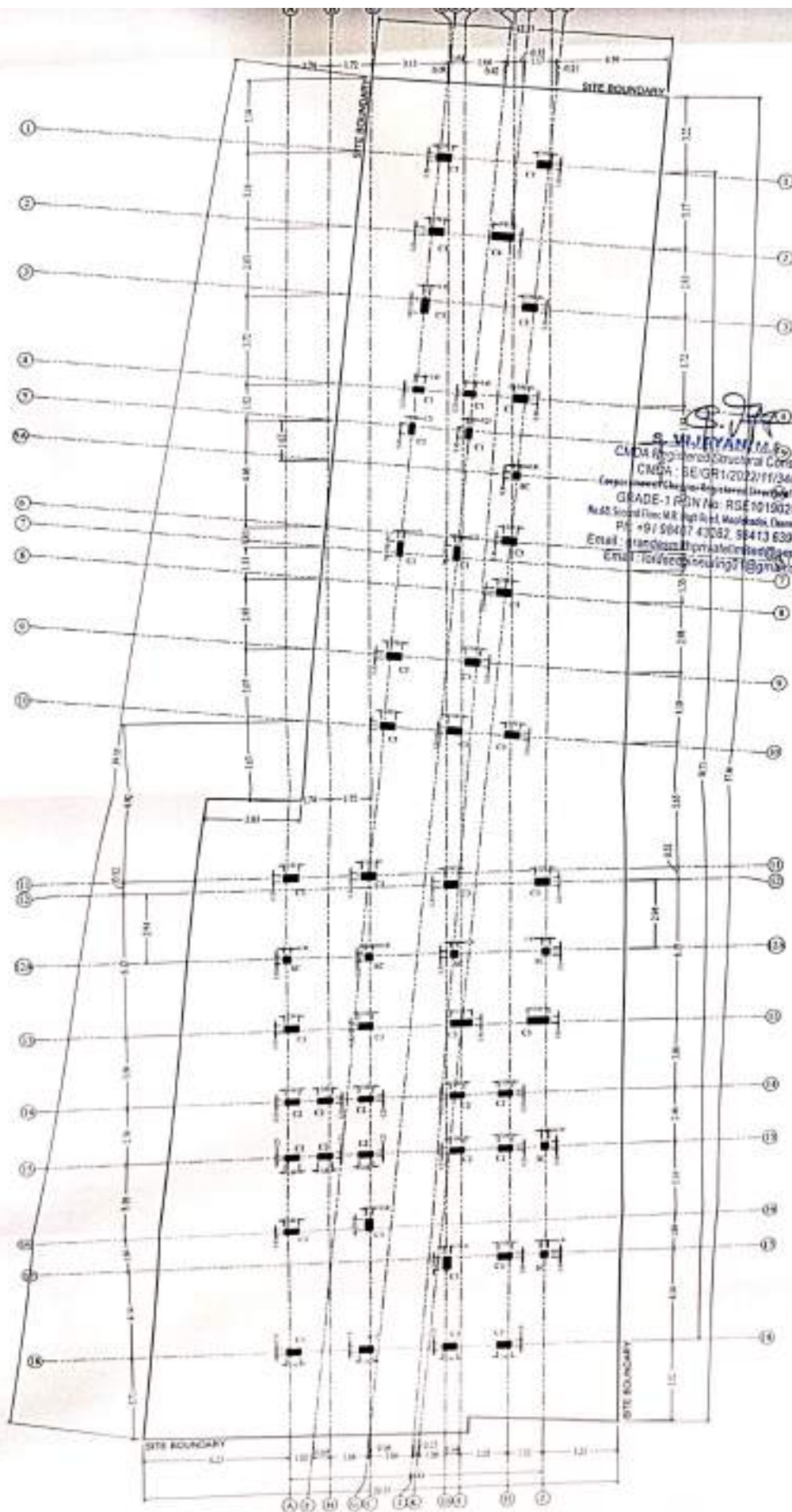


Superintending Engineer (Electrical)
Greater Chennai Corporation.

RGN No: RSE101902023
Dated: 08.01.2024

U. S. S. S.
08/01/24

08/01/24



- [illegible]

REFERENCES:

1. A SUMMARY OF THE ACTS AND REACTIONS OF THE CASE BEING NUMBERED
2. WITH THE FIRST WRITTEN MAIL, EXAMINE FOR CONTENTS IN THE COMMUNICATIONS AND REPORTS OF THE LINE AND LINE.
3. DO NOT SCALE THE ORIGINAL WRITTEN MATERIALS AND TO BE FOLLOWED
4. ALL INFORMATION AND ALL THE FIRST WRITTEN MAIL, EXAMINE FOR CONTENTS IN THE COMMUNICATIONS AND REPORTS OF THE LINE AND LINE.
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12. WITHIN 24 HOURS - 2000 FOR THE COMMUNICATIONS AND REPORTS

GENERAL NOTES

- OUR LIVES IN THE STRUCTURE, WITH JOURNAL
OF HUMAN RIGHTS AND JOURNAL OF THE
BLACK GLOBE, WE WOULD BE THE
COURTESY.

CLEAR COVER

1. COLUMN = 40mm.
2. ROOF BEAM = 25mm.
3. ROOF SLAB = 20mm.
4. GRADE BEAM = 25mm.
5. FOOTING BASE = 75mm.
6. Footing top = 50mm.

LEGEND

- LEGEND
 ■ RC COLUMN
 ■ 30 CONCRETE
 ■ 550 STEEL

1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100. 101. 102. 103. 104. 105. 106. 107. 108. 109. 110. 111. 112. 113. 114. 115. 116. 117. 118. 119. 120. 121. 122. 123. 124. 125. 126. 127. 128. 129. 130. 131. 132. 133. 134. 135. 136. 137. 138. 139. 140. 141. 142. 143. 144. 145. 146. 147. 148. 149. 150. 151. 152. 153. 154. 155. 156. 157. 158. 159. 160. 161. 162. 163. 164. 165. 166. 167. 168. 169. 170. 171. 172. 173. 174. 175. 176. 177. 178. 179. 180. 181. 182. 183. 184. 185. 186. 187. 188. 189. 190. 191. 192. 193. 194. 195. 196. 197. 198. 199. 200. 201. 202. 203. 204. 205. 206. 207. 208. 209. 210. 211. 212. 213. 214. 215. 216. 217. 218. 219. 220. 221. 222. 223. 224. 225. 226. 227. 228. 229. 230. 231. 232. 233. 234. 235. 236. 237. 238. 239. 240. 241. 242. 243. 244. 245. 246. 247. 248. 249. 250. 251. 252. 253. 254. 255. 256. 257. 258. 259. 260. 261. 262. 263. 264. 265. 266. 267. 268. 269. 270. 271. 272. 273. 274. 275. 276. 277. 278. 279. 280. 281. 282. 283. 284. 285. 286. 287. 288. 289. 290. 291. 292. 293. 294. 295. 296. 297. 298. 299. 300. 301. 302. 303. 304. 305. 306. 307. 308. 309. 310. 311. 312. 313. 314. 315. 316. 317. 318. 319. 320. 321. 322. 323. 324. 325. 326. 327. 328. 329. 330. 331. 332. 333. 334. 335. 336. 337. 338. 339. 340. 341. 342. 343. 344. 345. 346. 347. 348. 349. 350. 351. 352. 353. 354. 355. 356. 357. 358. 359. 360. 361. 362. 363. 364. 365. 366. 367. 368. 369. 370. 371. 372. 373. 374. 375. 376. 377. 378. 379. 380. 381. 382. 383. 384. 385. 386. 387. 388. 389. 390. 391. 392. 393. 394. 395. 396. 397. 398. 399. 400. 401. 402. 403. 404. 405. 406. 407. 408. 409. 410. 411. 412. 413. 414. 415. 416. 417. 418. 419. 420. 421. 422. 423. 424. 425. 426. 427. 428. 429. 430. 431. 432. 433. 434. 435. 436. 437. 438. 439. 440. 441. 442. 443. 444. 445. 446. 447. 448. 449. 450. 451. 452. 453. 454. 455. 456. 457. 458. 459. 460. 461. 462. 463. 464. 465. 466. 467. 468. 469. 470. 471. 472. 473. 474. 475. 476. 477. 478. 479. 480. 481. 482. 483. 484. 485. 486. 487. 488. 489. 490. 491. 492. 493. 494. 495. 496. 497. 498. 499. 500. 501. 502. 503. 504. 505. 506. 507. 508. 509. 510. 511. 512. 513. 514. 515. 516. 517. 518. 519. 520. 521. 522. 523. 524. 525. 526. 527. 528. 529. 530. 531. 532. 533. 534. 535. 536. 537. 538. 539. 540. 541. 542. 543. 544. 545. 546. 547. 548. 549. 550. 551. 552. 553. 554. 555. 556. 557. 558. 559. 560. 561. 562. 563. 564. 565. 566. 567. 568. 569. 570. 571. 572. 573. 574. 575. 576. 577. 578. 579. 580. 581. 582. 583. 584. 585. 586. 587. 588. 589. 590. 591. 592. 593. 594. 595. 596. 597. 598. 599. 600. 601. 602. 603. 604. 605. 606. 607. 608. 609. 610. 611. 612. 613. 614. 615. 616. 617. 618. 619. 620. 621. 622. 623. 624. 625. 626. 627. 628. 629. 630. 631. 632. 633. 634. 635. 636. 637. 638. 639. 640. 641. 642. 643. 644. 645. 646. 647. 648. 649. 650. 651. 652. 653. 654. 655. 656. 657. 658. 659. 660. 661. 662. 663. 664. 665. 666. 667. 668. 669. 670. 671. 672. 673. 674. 675. 676. 677. 678. 679. 680. 681. 682. 683. 684. 685. 686. 687. 688. 689. 690. 691. 692. 693. 694. 695. 696. 697. 698. 699. 700. 701. 702. 703. 704. 705. 706. 707. 708. 709. 710. 711. 712. 713. 714. 715. 716. 717. 718. 719. 720. 721. 722. 723. 724. 725. 726. 727. 728. 729. 730. 731. 732. 733. 734. 735. 736. 737. 738. 739. 740. 741. 742. 743. 744. 745. 746. 747. 748. 749. 750. 751. 752. 753. 754. 755. 756. 757. 758. 759. 760. 761. 762. 763. 764. 765. 766. 767. 768. 769. 770. 771. 772. 773. 774. 775. 776. 777. 778. 779. 780. 781. 782. 783. 784. 785. 786. 787. 788. 789. 790. 791. 792. 793. 794. 795. 796. 797. 798. 799. 800. 801. 802. 803. 804. 805. 806. 807. 808. 809. 810. 811. 812. 813. 814. 815. 816. 817. 818. 819. 820. 821. 822. 823. 824. 825. 826. 827. 828. 829. 830. 831. 832. 833. 834. 835. 836. 837. 838. 839. 840. 84

ARCHITECT
JC250688-NEXA-ASTA-(S+O3)
RESIDENTIAL BUILDING AT
MOGAPPAIR

DATE : 30.07.2025

| | |
|-------------|---------------------------------|
| NAME | FOR CONSTRUCTION FOR SODA STOPS |
| DESCRIPTION | DATE |

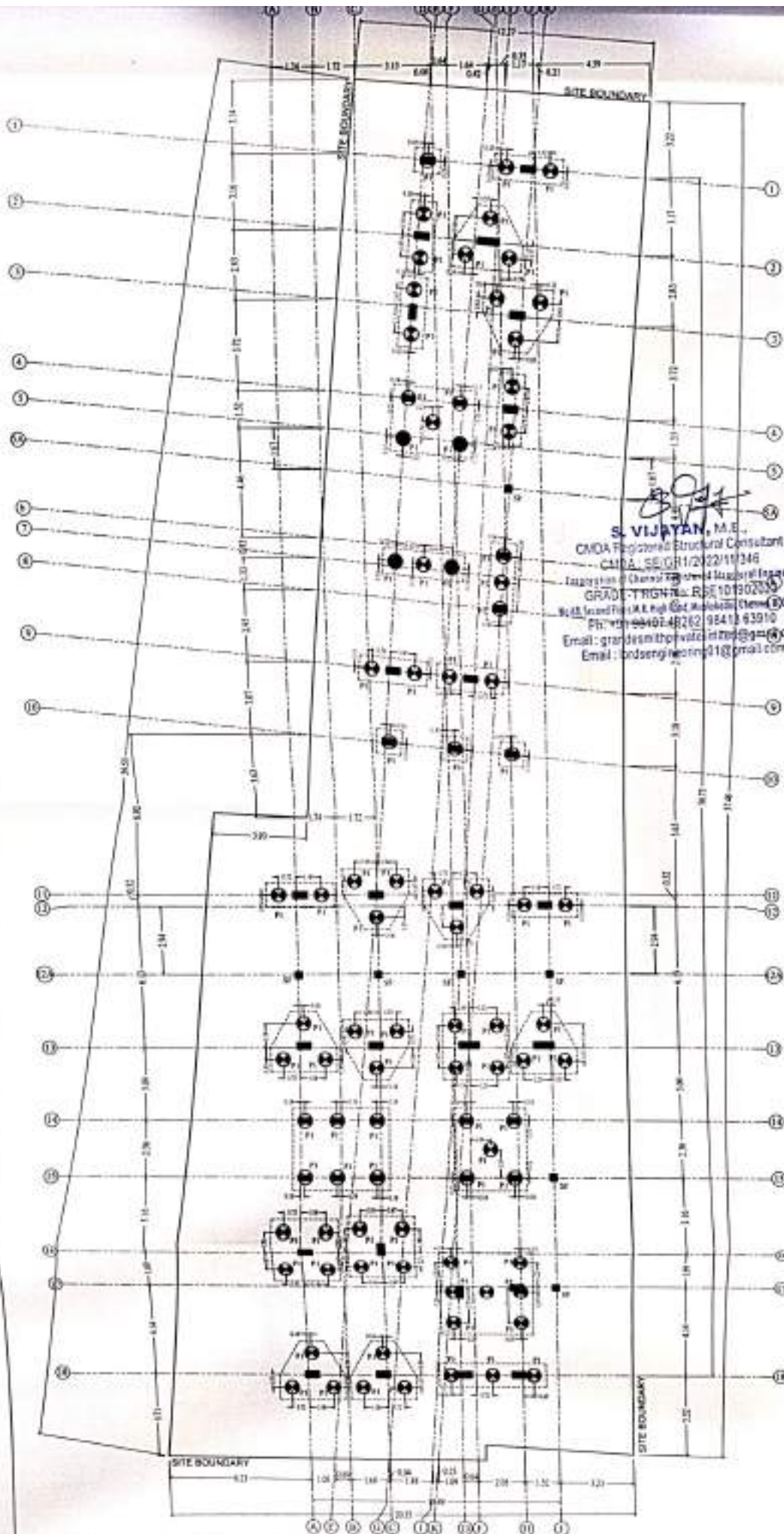
AMENDMENTS

| | |
|-----------------------------------|----------------------|
| TABLE: 6. MACE | SCALE: FT |
| Q634 BALAKRISHNAN, M | Q634 Balakrishnan, M |
| Q634 NQ | Q634 |
| Q634-ASTA-00024-STR-01-101 | Q634 |
| MONITORING - DESIGN - CONSULTANCY | |



**LORDS ENGINEERING
STRUCTURAL**
11/18, SECOND FLOOR, MADHAVARAM
REGHILL HIGHROAD, MOOLAKADAI,
PERAMBUR, CHENNAI-600 050.
-Mail: lordsengineering31@gmail.com
Mobile: +91 98407 43762

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|-----|------|----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | 101 | 102 | 103 | 104 | 105 | 106 | 107 | 108 | 109 | 110 | 111 | 112 | 113 | 114 | 115 | 116 | 117 | 118 | 119 | 120 | 121 | 122 | 123 | 124 | 125 | 126 | 127 | 128 | 129 | 130 | 131 | 132 | 133 | 134 | 135 | 136 | 137 | 138 | 139 | 140 | 141 | 142 | 143 | 144 | 145 | 146 | 147 | 148 | 149 | 150 | 151 | 152 | 153 | 154 | 155 | 156 | 157 | 158 | 159 | 160 | 161 | 162 | 163 | 164 | 165 | 166 | 167 | 168 | 169 | 170 | 171 | 172 | 173 | 174 | 175 | 176 | 177 | 178 | 179 | 180 | 181 | 182 | 183 | 184 | 185 | 186 | 187 | 188 | 189 | 190 | 191 | 192 | 193 | 194 | 195 | 196 | 197 | 198 | 199 | 200 | 201 | 202 | 203 | 204 | 205 | 206 | 207 | 208 | 209 | 210 | 211 | 212 | 213 | 214 | 215 | 216 | 217 | 218 | 219 | 220 | 221 | 222 | 223 | 224 | 225 | 226 | 227 | 228 | 229 | 230 | 231 | 232 | 233 | 234 | 235 | 236 | 237 | 238 | 239 | 240 | 241 | 242 | 243 | 244 | 245 | 246 | 247 | 248 | 249 | 250 | 251 | 252 | 253 | 254 | 255 | 256 | 257 | 258 | 259 | 260 | 261 | 262 | 263 | 264 | 265 | 266 | 267 | 268 | 269 | 270 | 271 | 272 | 273 | 274 | 275 | 276 | 277 | 278 | 279 | 280 | 281 | 282 | 283 | 284 | 285 | 286 | 287 | 288 | 289 | 290 | 291 | 292 | 293 | 294 | 295 | 296 | 297 | 298 | 299 | 300 | 301 | 302 | 303 | 304 | 305 | 306 | 307 | 308 | 309 | 310 | 311 | 312 | 313 | 314 | 315 | 316 | 317 | 318 | 319 | 320 | 321 | 322 | 323 | 324 | 325 | 326 | 327 | 328 | 329 | 330 | 331 | 332 | 333 | 334 | 335 | 336 | 337 | 338 | 339 | 340 | 341 | 342 | 343 | 344 | 345 | 346 | 347 | 348 | 349 | 350 | 351 | 352 | 353 | 354 | 355 | 356 | 357 | 358 | 359 | 360 | 361 | 362 | 363 | 364 | 365 | 366 | 367 | 368 | 369 | 370 | 371 | 372 | 373 | 374 | 375 | 376 | 377 | 378 | 379 | 380 | 381 | 382 | 383 | 384 | 385 | 386 | 387 | 388 | 389 | 390 | 391 | 392 | 393 | 394 | 395 | 396 | 397 | 398 | 399 | 400 | 401 | 402 | 403 | 404 | 405 | 406 | 407 | 408 | 409 | 410 | 411 | 412 | 413 | 414 | 415 | 416 | 417 | 418 | 419 | 420 | 421 | 422 | 423 | 424 | 425 | 426 | 427 | 428 | 429 | 430 | 431 | 432 | 433 | 434 | 435 | 436 | 437 | 438 | 439 | 440 | 441 | 442 | 443 | 444 | 445 | 446 | 447 | 448 | 449 | 450 | 451 | 452 | 453 | 454 | 455 | 456 | 457 | 458 | 459 | 460 | 461 | 462 | 463 | 464 | 465 | 466 | 467 | 468 | 469 | 470 | 471 | 472 | 473 | 474 | 475 | 476 | 477 | 478 | 479 | 480 | 481 | 482 | 483 | 484 | 485 | 486 | 487 | 488 | 489 | 490 | 491 | 492 | 493 | 494 | 495 | 496 | 497 | 498 | 499 | 500 | 501 | 502 | 503 | 504 | 505 | 506 | 507 | 508 | 509 | 510 | 511 | 512 | 513 | 514 | 515 | 516 | 517 | 518 | 519 | 520 | 521 | 522 | 523 | 524 | 525 | 526 | 527 | 528 | 529 | 530 | 531 | 532 | 533 | 534 | 535 | 536 | 537 | 538 | 539 | 540 | 541 | 542 | 543 | 544 | 545 | 546 | 547 | 548 | 549 | 550 | 551 | 552 | 553 | 554 | 555 | 556 | 557 | 558 | 559 | 560 | 561 | 562 | 563 | 564 | 565 | 566 | 567 | 568 | 569 | 570 | 571 | 572 | 573 | 574 | 575 | 576 | 577 | 578 | 579 | 580 | 581 | 582 | 583 | 584 | 585 | 586 | 587 | 588 | 589 | 590 | 591 | 592 | 593 | 594 | 595 | 596 | 597 | 598 | 599 | 600 | 601 | 602 | 603 | 604 | 605 | 606 | 607 | 608 | 609 | 610 | 611 | 612 | 613 | 614 | 615 | 616 | 617 | 618 | 619 | 620 | 621 | 622 | 623 | 624 | 625 | 626 | 627 | 628 | 629 | 630 | 631 | 632 | 633 | 634 | 635 | 636 | 637 | 638 | 639 | 640 | 641 | 642 | 643 | 644 | 645 | 646 | 647 | 648 | 649 | 650 | 651 | 652 | 653 | 654 | 655 | 656 | 657 | 658 | 659 | 660 | 661 | 662 | 663 | 664 | 665 | 666 | 667 | 668 | 669 | 670 | 671 | 672 | 673 | 674 | 675 | 676 | 677 | 678 | 679 | 680 | 681 | 682 | 683 | 684 | 685 | 686 | 687 | 688 | 689 | 690 | 691 | 692 | 693 | 694 | 695 | 696 | 697 | 698 | 699 | 700 | 701 | 702 | 703 | 704 | 705 | 706 | 707 | 708 | 709 | 710 | 711 | 712 | 713 | 714 | 715 | 716 | 717 | 718 | 719 | 720 | 721 | 722 | 723 | 724 | 725 | 726 | 727 | 728 | 729 | 730 | 731 | 732 | 733 | 734 | 735 | 736 | 737 | 738 | 739 | 740 | 741 | 742 | 743 | 744 | 745 | 746 | 747 | 748 | 749 | 750 | 751 | 752 | 753 | 754 | 755 | 756 | 757 | 758 | 759 | 760 | 761 | 762 | 763 | 764 | 765 | 766 | 767 | 768 | 769 | 770 | 771 | 772 | 773 | 774 | 775 | 776 | 777 | 778 | 779 | 780 | 781 | 782 | 783 | 784 | 785 | 786 | 787 | 788 | 789 | 790 | 791 | 792 | 793 | 794 | 795 | 796 | 797 | 798 | 799 | 800 | 801 | 802 | 803 | 804 | 805 | 806 | 807 | 808 | 809 | 810 | 811 | 812 | 813 | 814 | 815 | 816 | 817 | 818 | 819 | 820 | 821 | 822 | 823 | 824 | 825 | 826 | 827 | 828 | 829 | 830 | 831 | 832 | 833 | 834 | 835 | 836 | 837 | 838 | 839 | 840 | 841 | 842 | 843 | 844 | 845 | 846 | 847 | 848 | 849 | 850 | 851 | 852 | 853 | 854 | 855 | 856 | 857 | 858 | 859 | 860 | 861 | 862 | 863 | 864 | 865 | 866 | 867 | 868 | 869 | 870 | 871 | 872 | 873 | 874 | 875 | 876 | 877 | 878 | 879 | 880 | 881 | 882 | 883 | 884 | 885 | 886 | 887 | 888 | 889 | 890 | 891 | 892 | 893 | 894 | 895 | 896 | 897 | 898 | 899 | 900 | 901 | 902 | 903 | 904 | 905 | 906 | 907 | 908 | 909 | 910 | 911 | 912 | 913 | 914 | 915 | 916 | 917 | 918 | 919 | 920 | 921 | 922 | 923 | 924 | 925 | 926 | 927 | 928 | 929 | 930 | 931 | 932 | 933 | 934 | 935 | 936 | 937 | 938 | 939 | 940 | 941 | 942 | 943 | 944 | 945 | 946 | 947 | 948 | 949 | 950 | 951 | 952 | 953 | 954 | 955 | 956 | 957 | 958 | 959 | 960 | 961 | 962 | 963 | 964 | 965 | 966 | 967 | 968 | 969 | 970 | 971 | 972 | 973 | 974 | 975 | 976 | 977 | 978 | 979 | 980 | 981 | 982 | 983 | 984 | 985 | 986 | 987 | 988 | 989 | 990 | 991 | 992 | 993 | 994 | 995 | 996 | 997 | 998 | 999 | 1000 | 1001 | 1002 | 1003 | 1004 | 1005 | 1006 | 1007 | 1008 | 1009 | 1010 | 1011 | 1012 | 1013 | 1014 | 1015 | 1016 | 1017 | 1018 | 1019 | 1020 | 1021 | 1022 | 1023 | 1024 | 1025 | 1026 | 1027 | 1028 | 1029 | 1030 | 1031 | 1032 | 1033 | 1034 | 1035 | 1036 | 1037 | 1038 | 1039 | 1040 | 1041 | 1042 | 1043 | 1044 | 1045 | 1046 | 1047 | 1048 | 1049 | 1050 | 1051 | 1052 | 1053 | 1054 | 1055 | 1056 | 1057 | 1058 | 1059 | 1060 | 1061 | 1062 | 1063 | 1064 | 1065 | 1066 | 1067 | 1068 | 1069 | 1070 | 1071 | 1072 | 1073 | 1074 | 1075 | 1076 | 1077 | 1078 | 1079 | 1080 | 1081 | 1082 | 1083 | 1084 | 1085 | 1086 | 1087 | 1088 | 1089 | 1090 | 1091 | 1092 | 1093 | 1094 | 1095 | 1096 | 1097 | 1098 | 1099 | 1100 | 1101 | 1102 | 1103 | 1104 | 1105 | 1106 | 1107 | 1108 | 1109 | 1110 | 1111 | 1112 | 1113 | 1114 | 1115 | 1116 | 1117 | 1118 | 1119 | 1120 | 1121 | 1122 | 1123 | 1124 | 1125 | 1126 | 1127 | 1128 | 1129 | 1130 | 1131 | 1132 | 1133 | 1134 | 1135 | 1136 | 1137 | 1138 | 1139 | 1140 | 1141 | 1142 | 1143 | 1144 | 1145 | 1146 | 1147 | 1148 | 1149 | 1150 | 1151 | 1152 | 1153 | 1154 | 1155 | 1156 | 1157 | 1158 | 1159 | 1160 | 1161 | 1162 | 1163 | 1164 | 1165 | 1166 | 1167 | 1168 | 1169 | 1170 | 1171 | 1172 | 1173 | 1174 | 1175 | 1176 | 1177 | 1178 | 1179 | 1180 | 1181 | 1182 | 1183 | 1184 | 1185 | 1186 | 1187 | 1188 | 1189 | 1190 | 1191 | 1192 | 1193 | 1194 | 1195 | 1196 | 1197 | 1198 | 1199 | 1200 | 1201 | 1202 | 1203 | 1204 | 1205 | 1206 | 1207 | 1208 | 1209 | 1210 | 1211 | 1212 | 1213 | 1214 | 1215 | 1216 | 1217 | 1218 | 1219 | 1220 | 1221 | 1222 | 1223 | 1224 | 1225 | 1226 | 1227 | 1228 | 1229 | 1230 | 1231 | 1232 | 1233 | 1234 | 1235 | 1236 | 1237 | 1238 | 1239 | 1240 | 1241 | 1242 | 1243 | 1244 | 1245 | 1246 | 1247 | 1248 | 1249 | 1250 | 1251 | 1252 | 1253 | 1254 | 1255 | 1256 | 1257 | 1258 | 1259 | 1260 | 1261 | 1262 | 1263 | 1264 | 1265 | 1266 | 1267 | 1268 | 1269 | 1270 | 1271 | 1272 | 1273 | 1274 | 1275 | 1276 | 1277 | 1278 | 1279 | 1280 | 1281 | 1282 | 1283 | 1284 | 1285 | 1286 | 1287 | 1288 | 1289 | 1290 | 1291 | 1292 | 1293 | 1294 | 1295 | 1296 | 1297 | 1298 | 1299 | 1300 | 1301 | 1302 | 1303 | 1304 | 1305 | 1306 | 1307 | 1308 | 1309 | 1310 | 1311 | 1312 | 1313 | 1314 | 1315 | 1316 | 1317 | 1318 | 1319 | 1320 | 1321 | 1322 | 1323 | 1324 | 1325 | 1326 | 1327 | 1328 | 1329 | 1330 | 1331 | 1332 | 1333 | 1334 | 1335 | 1336 | 1337 | 1338 | 1339 | 1340 | 1341 | 1342 | 1343 | 1344 | 1345 | 1346 | 1347 | 1348 | 1349 | 1350 | 1351 | 1352 | 1353 | 1354 | 1355 | 1356 | 1357 | 1358 | 1359 | 1360 | 1361 | 1362 | 1363 | 1364 | 1365 | 1366 | 1367 | 1368 | 1369 | 1370 | 1371 | 1372 | 1373 | 1374 | 1375 | 1376 | 1377 | 1378 | 1379 | 1380 | 1381 | 1382 | 1383 | 1384 | 1385 | 1386 | 1387 | 1388 | 1389 | 1390 | 1391 | 1392 | 1393 | 1394 | 1395 | 1396 | 1397 | 1398 | 1399 | 1400 | 1401 | 1402 | 1403 | 1404 | 1405 | 1406 | 1407 | 1408 | 1409 | 1410 | 1411 | 1412 | 1413 | 1414 | 1415 | 1416 | 1417 | 1418 | 1419 | 1420 | 1421 | 1422 | 1423 | 1424 | 1425 | 1426 | 1427 | 1428 | 1429 | 1430 | 1431 | 1432 | 1433 | 1434 | 1435 | 1436 | 1437 | 1438 | 1439 | 1440 | 1441 | 1442 | 1443 | 1444 | 1445 | 1446 | 1447 | 1448 | 1449 | 1450 | 1451 | 1452 | 1453 | 1454 | 1455 | 1456 | 1457 | 1458 | 1459 | 1460 | 1461 | 1462 | 1463 | 1464 | 1465 | 1466 | 1467 | 1468 | 1469 | 1470 | 1471 | 1472 | 1473 | 1474 | 1475 | 1476 | 1477 | 1478 | 1479 | 1480 | 1481 | 1482 | 1483 | 1484 | 1485 | 1486 | 1487 | 1488 | 1489 | 1490 | 1491 | 1492 | 1493 | 1494 | 1495 | 14 |
|---|---|---|---|---|---|---|---|---|-----|------|----|



1. ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SPECIFIED.
2. THE PILE GRID MARKING SHALL BE DONE FOR ALL CONCRETE WORK.
3. GRADE APPROPRIATE FOR SHALL BE DONE FOR ALL CONCRETE WORK.
4. MINIMUM GRADE SHALL BE 100mm BELOW FINISHED FLOOR LEVEL.
5. OVER SAND SHALL BE MAINTAINED AND SHOULD BE REMOVED DURING CONSTRUCTION.
6. PROPER DETAILING OF CONCRETE SHALL BE PROVIDED THROUGHOUT THE ENTIRE WORK AND THE SAME SHALL BE FOLLOWED THROUGHOUT THE CONSTRUCTION.
7. COMPRESSION STRENGTH OF CONCRETE SHALL BE TESTED DURING CONSTRUCTION FOR ALL COMPONENTS OF THE BUILDING AND RECORDS.
8. WATER SHALL BE OF GOOD QUALITY AND IT SHALL BE TESTED IN A REPUTABLE LABORATORY TO ASCERTAIN THE SUITABILITY FOR CONCRETE WORK.
9. CURING OF CONCRETE STRUCTURES BY APPROPRIATE METHOD SHALL BE SUPERINTENDED TO ACHIEVE THE DESIRED DESIGN STRENGTH.

REFERENCES:

1. ALWAYS REFER THE LATEST EDITION OF THE IS CODES.
2. REFER RELEVANT ARCHITECTURAL DRAWINGS FOR CORRECT BUILDING COMPONENT MEASUREMENTS, DIMENSIONS AND LEVELS.
3. DO NOT SCALE THE DRAWING. WRITTEN DIMENSIONS ARE TO BE FOLLOWED.
4. ALL DIMENSIONS ARE IN METERS UNLESS OTHERWISE SPECIFIED. MEASUREMENTS IN METERS ARE TO BE TAKEN ALONG THE LINES, UNLESS OTHERWISE SPECIFIED.
5. REFER IS 456 - 2000 FOR RCC CONSTRUCTION AND PRACTICE.
6. REFER IS 5925 - 2004 FOR REINFORCEMENT DETAILING IN RCC STRUCTURES.
7. REFER IS 456 - 2000 FOR RCC CONSTRUCTION AND PRACTICE.
8. REFER IS 5925 - 2004 FOR REINFORCEMENT DETAILING IN RCC STRUCTURES.
9. REFER IS 2911 - 1987 FOR PILE FOUNDATION.
10. REFER IS 3370 - 2004 FOR CONCRETE STRUCTURES FOR LOADS AT RAKE.
11. REFER IS 800 - 2007 FOR STEEL STRUCTURAL DESIGN IN CONSTRUCTION.

GENERAL NOTES

1. OVER LOADING OF THE STRUCTURE WITH QUANTITY OF MATERIALS AND EQUIPMENTS AT ONE PLACE SHALL BE AVOIDED DURING THE CONSTRUCTION.
2. USE OF LOW STRENGTH CONCRETE FOR PILES IS NOT RECOMMENDED UNLESS OTHERWISE SPECIFIED IN THE DESIGN.
3. USE OF LOW STRENGTH MATERIAL CONCRETE IS NOT RECOMMENDED FOR PILING OF PILES.

CLEAR COVER

1. COLUMN = 40mm.
2. ROOF BEAM = 25mm.
3. ROOF SLAB = 20mm.
4. GRADE BEAM = 25mm.
5. FOOTING BASE = 75mm.
6. FOOTING SIDE = 50mm.

LEGEND

- RC COLUMN
- M 30 CONCRETE
- F 550 STEEL

ARCHITECT

JC250688-NEXA-ASTA-(S+03)
RESIDENTIAL BUILDING AT
MOGAPPUR

DATE : 30.07.2025

| | | |
|-----|-------------------------|------------|
| REV | DESCRIPTION | DATE |
| 01 | ISSUED FOR CONSTRUCTION | 30.07.2025 |

AMENDMENTS

| | |
|---------------------------------------|------------------|
| DESIGNED BY: K. MADHURAN | SCALE: 1:100 |
| CHECKED BY: BALAKRISHNAN M | DATE: 30.07.2025 |
| DRAWING NO: NEXA-ASTA-MOGA-SRU-01-003 | REV: 00 |
| ENGINEERING - DESIGN - CONSULTANCY | |



LORDS ENGINEERING STRUCTURAL

No.68, SECOND FLOOR, MADHAVARAU
REDHILLS, HIGHROAD, MOOLAKADAI,
PERAMBUR, CHENNAI-600 060.
E-Mail: lordsengineering01@gmail.com
Mobile: +91 98407 43262

| | | | |
|-------|--------------------------|----------|----------|
| TITLE | PILE GRID MARKING LAYOUT | LOCATION | MOGAPPUR |
|-------|--------------------------|----------|----------|

| | | | | |
|-------|----------------------|----------|-----------|---|
| TITLE | PILE SECTION DETAILS | LOCATION | MOGAPPAIR | E-Mail: hrdipeng@redgig01@gmail.com
Mobile: +91 95427 43262 |
|-------|----------------------|----------|-----------|---|

PILE CAP SCHEDULE (M30:Fe550)

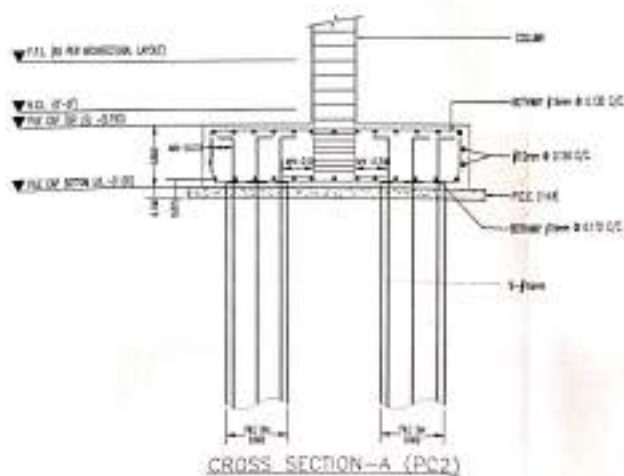
| PILE CAP
MARK | PILES | DIMENSIONS (m) | | | REINFORCEMENT | | | |
|------------------|---------|----------------|--------|-----|---------------|-------------|-------------|-------------|
| | | L | B | D | BOTTOM | | TOP | |
| | | | | | ALONG L | ALONG B | ALONG L | ALONG B |
| PC1 | 600 DIA | 1.06 | 1.06 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC2 | 600 DIA | 2.86 | 1.06 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC3 | 600 DIA | AS PER | AS PER | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC4 | 600 DIA | 2.86 | 2.86 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC5 | 600 DIA | 3.42 | 1.04 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC6 | 600 DIA | 3.24 | 1.06 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC7 | 600 DIA | 4.66 | 1.06 | 1.0 | T16@150 C/C | T16@150 C/C | T12@180 C/C | T12@150 C/C |
| PC8 | 600 DIA | 3.42 | 2.70 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC9 | 600 DIA | 3.12 | 3.42 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC10 | 600 DIA | 4.16 | 3.42 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |
| PC11 | 600 DIA | 4.00 | 4.00 | 1.0 | T16@150 C/C | T16@150 C/C | T12@150 C/C | T12@150 C/C |

NOTE: PILECAP DEPTH
PILECAP DEPTH FROM NGL TO
BOTTOM OF THE PILECAP: 1m

[illegible]

| TECHNICAL SPECIFICATIONS | |
|--------------------------|----------------------|
| 1. Material | As per specification |
| 2. Quantity | As per drawing |
| 3. Location | As per drawing |
| 4. Date | As per drawing |
| 5. Drawn by | As per drawing |
| 6. Checked by | As per drawing |
| 7. Approved by | As per drawing |
| 8. Scale | As per drawing |
| 9. Notes | As per drawing |
| 10. Remarks | As per drawing |
| 11. Revision | As per drawing |
| 12. Drawing No. | As per drawing |
| 13. Project No. | As per drawing |
| 14. Client Name | As per drawing |
| 15. Site Name | As per drawing |
| 16. Drawing Date | As per drawing |
| 17. Drawing Scale | As per drawing |
| 18. Drawing Title | As per drawing |
| 19. Drawing Author | As per drawing |
| 20. Drawing Checker | As per drawing |
| 21. Drawing Approver | As per drawing |
| 22. Drawing Date | As per drawing |
| 23. Drawing Scale | As per drawing |
| 24. Drawing Title | As per drawing |
| 25. Drawing Author | As per drawing |
| 26. Drawing Checker | As per drawing |
| 27. Drawing Approver | As per drawing |
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| PROJECT | JC250688B-NEXA-ASTA-(S+05) | SITE | MAGAPPAIR | TITLE | PILE CAP REINFORCEMENT SCHEDULE |
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TECHNICAL SPECIFICATIONS

REFERENCES

GENERAL NOTES

CLEAR COVER

LEFEND

■ RC COLUMN
■ M30 CONCRETE
■ F-600 STEEL

ARCHITECT

UC250688-NEXA-ASTA-(S+O3)
RESIDENTIAL BUILDING AT
MOCAPPAIR

DATE : 30.07.2025

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LODS ENGINEERING
 401 N. 102nd Ave., Suite 100
 Minneapolis, MN 55431
 Tel: 763.771.1111
 Fax: 763.771.1112
 Email: info@lodsengineering.com
 Website: www.lodsengineering.com

1. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.

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REFERENCES:

1. IS 456:2000 FOR CONCRETE DESIGN AND CONSTRUCTION.
2. IS 800:2008 FOR STEEL DESIGN AND CONSTRUCTION.
3. IS 1786:2005 FOR REINFORCEMENT BARS.
4. IS 1920:2005 FOR CONCRETE TESTING METHODS.
5. IS 3952:2005 FOR CONCRETE TESTING METHODS.
6. IS 456:2000 FOR CONCRETE DESIGN AND CONSTRUCTION.
7. IS 800:2008 FOR STEEL DESIGN AND CONSTRUCTION.
8. IS 1786:2005 FOR REINFORCEMENT BARS.
9. IS 1920:2005 FOR CONCRETE TESTING METHODS.
10. IS 3952:2005 FOR CONCRETE TESTING METHODS.

GENERAL NOTES:

1. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.
2. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.
3. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.
4. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.
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8. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.
9. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.
10. THE DRAWING IS TO BE USED FOR CONSTRUCTION OF THE BUILDING.

CLEAR COVER

1. COLUMN = 40mm.
2. ROOF BEAM = 25mm.
3. ROOF SLAB = 20mm.
4. GRADE BEAM = 25mm.
5. FOOTING BASE = 75mm.
6. FOOTING SID = 50mm.

LEGEND

- RC COLUMN
- M 30 CONCRETE
- FY 550 STEEL

ARCHITECT

JC250688-NEXA-ASTA-(S+03)
RESIDENTIAL BUILDING AT
MOGAPPAIR

DATE : 30.07.2025

| | | |
|-----|-------------------------|------------|
| NO. | REVISION | DATE |
| 01 | ISSUED FOR CONSTRUCTION | 30.07.2025 |

AMENDMENTS

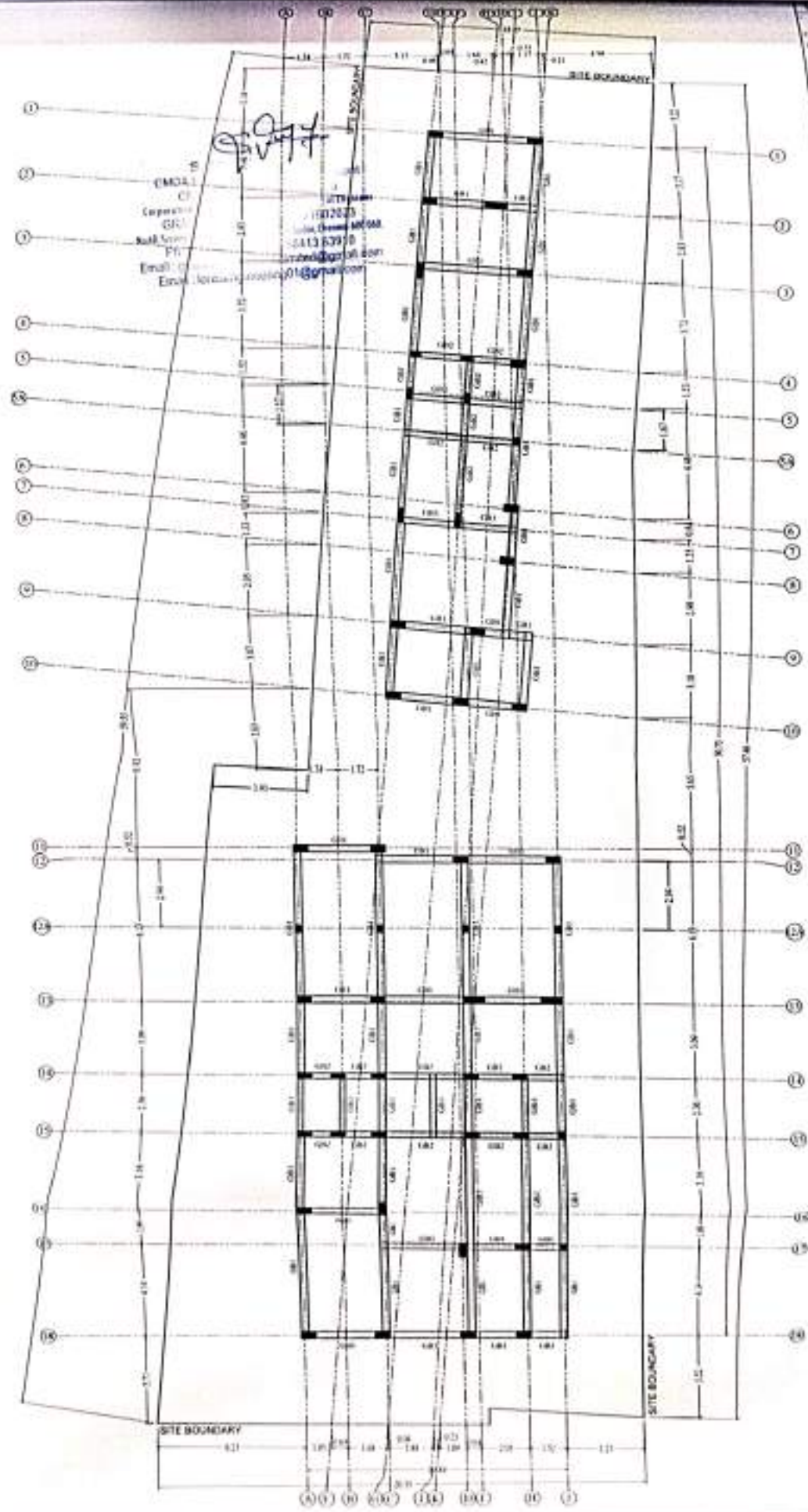
| | | |
|--------------|------------|-----|
| REVISION NO. | DATE | BY |
| 01 | 30.07.2025 | 001 |
| 02 | 30.07.2025 | 001 |

ENGINEERING - DESIGN - CONSULTANCY



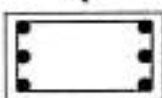
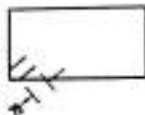
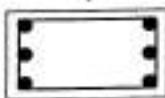
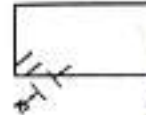
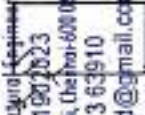
**LORDS ENGINEERING
STRUCTURAL**

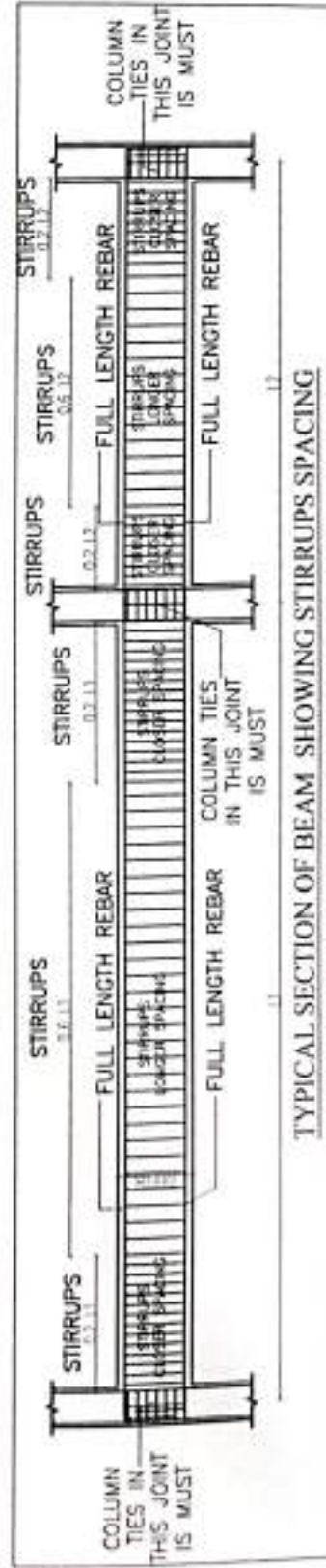
No. 05, SECOND FLOOR, MADHURAM
REDHILLS HIGHROAD, MOGAPPAIR,
PERAMBUR, CHENNAI-600 060
E-Mail: lordsengineering07@gmail.com
Mobile: 978 5637 5262



| | | | |
|-------|---------------------------|----------|-----------|
| TITLE | GRADE BEAM MARKING LAYOUT | LOCATION | MOGAPPAIR |
|-------|---------------------------|----------|-----------|

GRADE BEAM SCHEDULE

| TYPE | BEAM SIZE | GRADE BEAM REINFORCEMENT | | | | STIRRUP SHAPE |
|------|-----------|---|--|---|--|---|
| | | AT COLUMN JUNCTION | | AT MID SPAN | | |
| | | MAIN REIN. | VERTICAL STIRRUPS
FOR A LENGTH=0.2L | GRADE BEAM
CROSS SECTION | VERTICAL STIRRUPS
FOR A LENGTH=0.6L | |
| GB1 | 300X450 | FOR FULL LENGTH
● 3NOSx16mm dia | FOR A LENGTH=0.2L
8mm# @ 120mm C/C | 
450
300 | FOR A LENGTH=0.6L
8mm# @ 150mm C/C | 
8 mm DIA |
| | | FOR FULL LENGTH
● 3NOSx16mm dia | | | | |
| GB2 | 230X450 | FOR FULL LENGTH
● 3NOSx16mm dia | FOR A LENGTH=0.2L
8mm# @ 120mm C/C | 
450
230 | FOR A LENGTH=0.6L
8mm# @ 150mm C/C | 
8 mm DIA |
| | | FOR FULL LENGTH
● 3NOSx16mm dia | | | | |
| GB3 | 230X450 | FOR FULL LENGTH
○ 2NOSx12mm dia
● 1NOSx16mm dia | FOR A LENGTH=0.2L
8mm# @ 120mm C/C | 
450
230 | FOR A LENGTH=0.6L
8mm# @ 150mm C/C | 
8 mm DIA |
| | | FOR FULL LENGTH
○ 2NOSx12mm dia
● 1NOSx16mm dia | | | | |



NO CRANKING OF RODS IS REQUIRED - ALL RODS ARE STRAIGHT - AT TOP AND BOTTOM
NO CURTAILMENT OF MAIN RODS IS MENTIONED - ALL RODS ARE FULL LENGTH.
TOP REINFORCEMENT OF CANTILEVER BEAMS AS WELL AS RECTANGULAR BEAMS
SHALL NOT BE LAPPED.

| PROJECT | SITE | TITLE | GRADE BEAM REINFORCEMENT SCHEDULE |
|---------------------------|-----------|-------|-----------------------------------|
| JC250688-NEXA-ASTA-(S+05) | MACAPPAIR | | |

[illegible]